

# **Chemical Properties and Formation Mechanisms of Volatile Nanoparticles from LDV**

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## **1. INTRODUCTION**

Nanoparticles formed in vehicle exhaust have received increasing attention due to their potential adverse health effects. It has been reported that there are carbonaceous nanoparticles and volatile nanoparticles (nucleation particles) observed in urban air and the vehicle exhaust, and nucleation particles consist mainly of organic and sulfur compounds. The nucleation particles exhausted from vehicles have been observed under idling, deceleration and high load conditions. But there are a lot of uncertain points for chemical properties and formation mechanisms of the nucleation particles.

We have conducted engine bench test, theoretical simulation and chemical analysis to clarify the formation mechanism of the nucleation particles under idling condition in a light-duty diesel engine system.

## **2. EXPERIMENTAL METHODS**

Our engine system is a light-duty common-rail type DI diesel engine installing an oxidation catalyst and is controlled by a dynamometer. All experiments were performed at steady state. Engine-out and catalyst-out emissions were diluted by a NanoMet diluter and particle size distributions were measured by a SMPS.

In order to realize the chemical properties of the nucleation particles, we diluted the engine-out emissions under idling condition using a 2 stage-diluter and the diluted particles were classified by using a MOUDI and nano-MOUDI, and the size-classified particles were analyzed by using EPMA, FT-IR, GC-MS and TOF-SIMS.

We used three fundamental equations that treated nucleation, coagulation, condensation and vaporization to simulate the formation of nucleation particles at idle.

## **3. RESULTS and DISCUSSION**

The number concentration of the nucleation particles at idle was dependent strongly on fuel property. The nucleation particles at idle were composed mainly of more than C18 hydrocarbons in fuel and existed at the exhaust gas temperature that exceeded 100 degree C in an exhaust-pipe before

tailpipe-end and exhaust plume.

On the basis of the experimental result, we simulated the formation of the nucleation particles in the exhaust-pipe under idling condition. The result of simulation which treated the nucleation of  $C_{26}H_{54}$  on behalf of fuel elements was in disagreement with the experimental result. The nucleation materials must have lower vapor pressure and lower surface tension than those of  $C_{26}$  n-paraffin to obtain an enough nucleation rate. Considering the existence of the nucleation material whose vapor pressure was 1/10,000 and surface tension was 70% to those of  $C_{26}H_{54}$ , we could simulate the formation of the nucleation particles in the exhaust-pipe under idling condition.

In order to study the existence of the nucleation materials which had the specific physical properties derived from the theoretical simulation, particles observed at idle were classified and the size-classified particles were analyzed.

Through FT-IR analysis, oxygenated hydrocarbons and phosphate were detected mainly in the range of 10-56nm in diameter, although hydrocarbons were observed in all the diameter ranges.

Based on the result of FT-IR analysis, we performed detailed analysis with TOF-SIMS. The percentage content of C-H-O hetero-compounds increased with the decrease in the range of the nanoparticle diameter. The hetero-compounds were estimated to be low temperature oxidation products which had the skeleton of high mass number fuel hydrocarbons and would be one of the nucleation materials under idling condition.

The percentage contents of Zn and phosphate increased in the nanoparticle diameter ranges. Zn and phosphate was estimated to be pyrolytic products of Zn-DTP oil additive. We evaluated a formation characteristic of the nucleation particles by the use of both engine oil containing the additives and that not containing the additives. The presence of the oil additives did not influence the formation of the nucleation particles under idling condition. The pyrolytic products of Zn-DTP oil additive would have low vapor pressure but were not the nucleation materials.

#### 4. SUMMARY

We clarified the formation mechanism of the nucleation particles under idling condition in the light-duty diesel engine system.

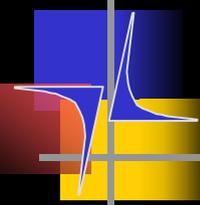
The nucleation of the C-H-O hetero-compounds (oxygenated hydrocarbons) of fuel origin proceeds at the exhaust gas temperature that exceeds 100 degree C in the exhaust-pipe and the nucleation particles at idle are formed by the condensation of high boiling point hydrocarbons of fuel elements to nucleus. The nucleation particles at idle consist of a small amount of the oxygenated hydrocarbons of fuel origin and a large amount of more than  $C_{18}$  hydrocarbons of fuel elements.



# Chemical Properties and Formation Mechanism of Volatile Nanoparticles from LDV

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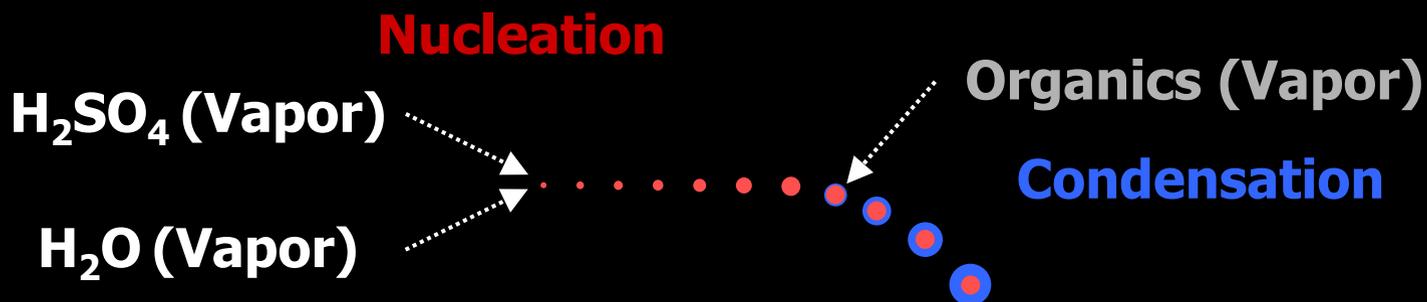
# Introduction

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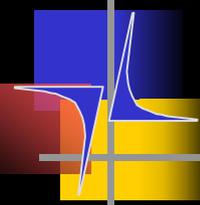
- Nucleation particles were observed under following engine operation conditions.
  - Idling (non-load) condition
  - Deceleration condition
  - High load condition  
(with high S fuel and/or oxidation catalyst)
- But there are a lot of uncertain points for chemical properties and formation mechanisms of nucleation particles.

# Nucleation Theory

- Formation mechanism of nucleation particles observed under high load conditions would be explained by  $\text{H}_2\text{SO}_4$ - $\text{H}_2\text{O}$  binary homogeneous nucleation (BHN) theory.



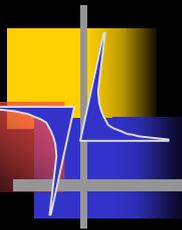
- In the case of idling and deceleration conditions, formation mechanisms of nucleation particles have not been explained theoretically yet.



# Objective and Approach

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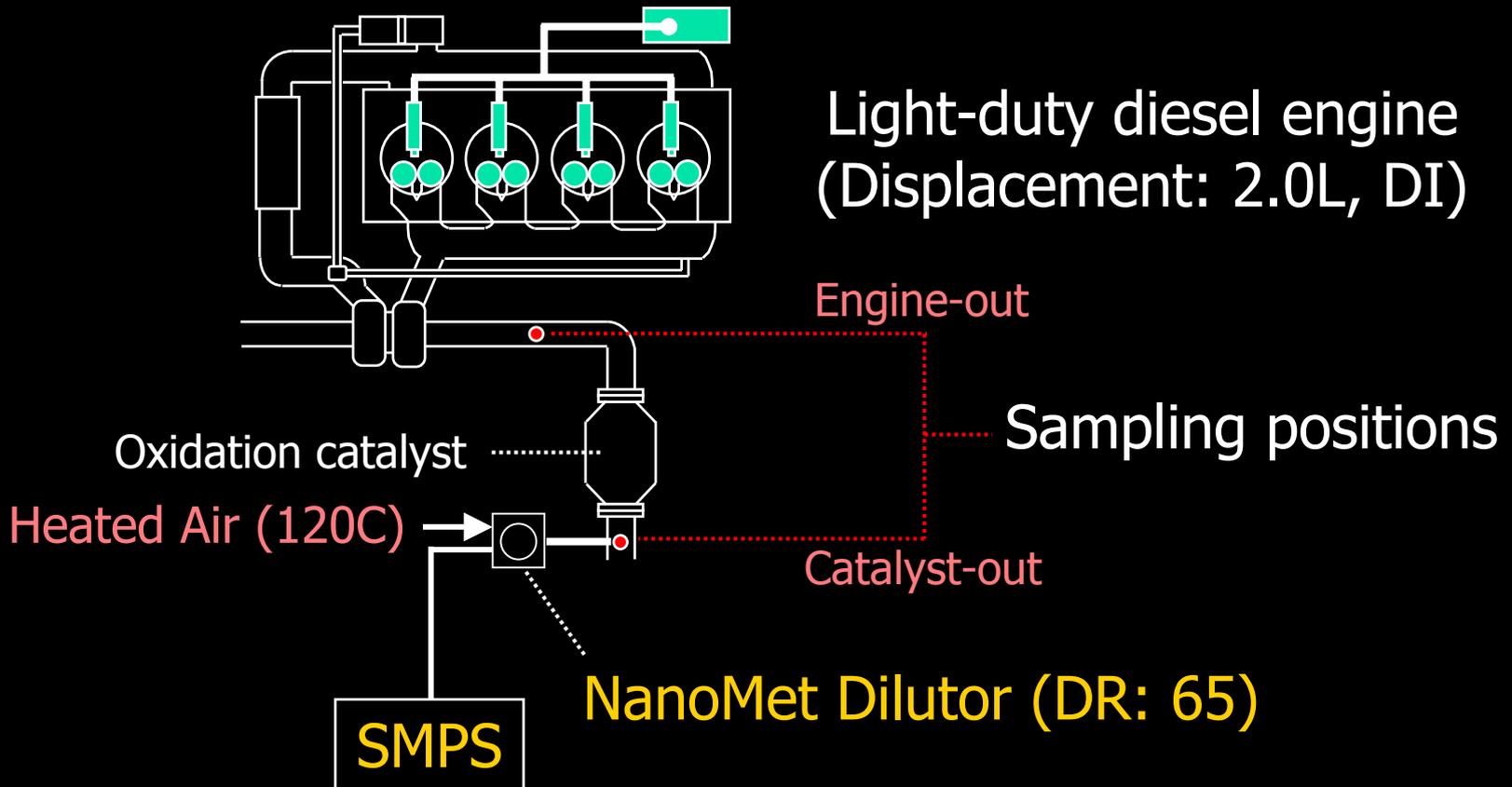
- To clarify formation mechanism of nucleation particles under idling condition through following approaches.
  - Engine bench test
  - Simulation of nucleation particle formation
  - Chemical analysis of nucleation particles

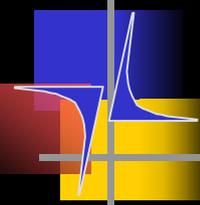


# 1. Engine bench test

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# Diesel Engine Experiment



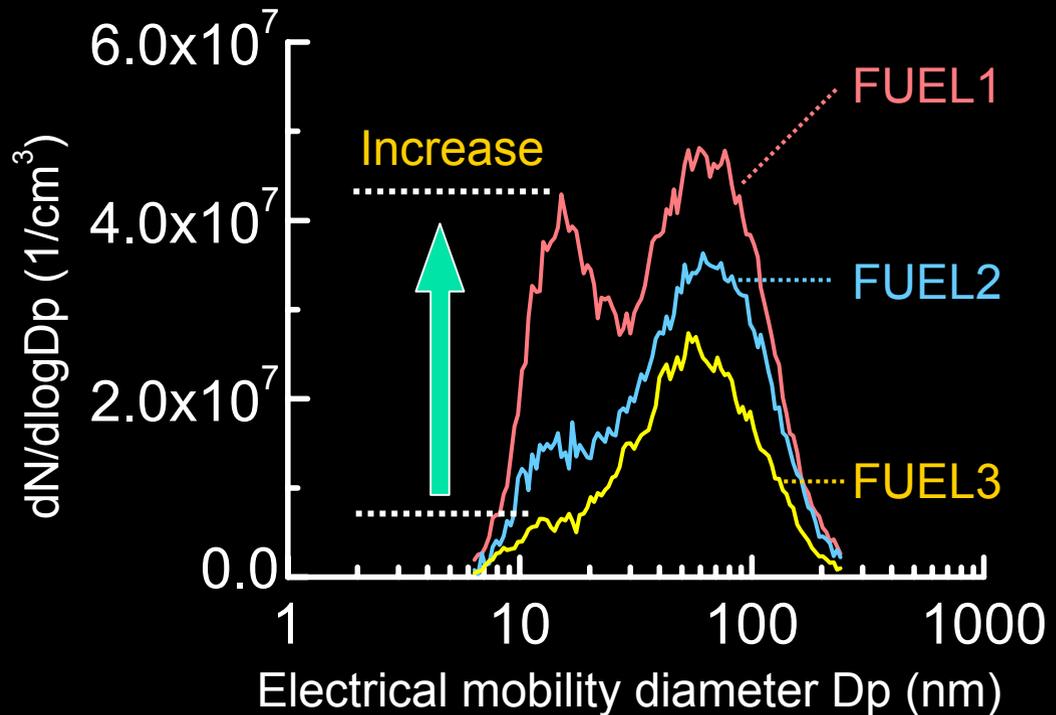
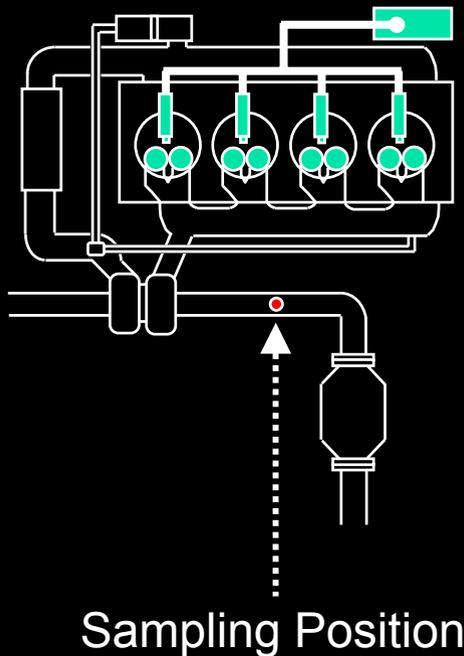


# Diesel Fuel Specifications

|                      | FUEL1<br>(High S) | FUEL2<br>(Conventional) | FUEL3<br>(Swedish Class 1) |
|----------------------|-------------------|-------------------------|----------------------------|
| Density @15deg C     | 0.8312            | 0.8323                  | 0.810                      |
| Cetane Index         | 55                | 53                      | 51.9                       |
| Aromatics vol%       | 27.6              | 18.5                    | 2.4                        |
| Sulfur mass ppm      | 430               | 28                      | 4                          |
| Distillation (deg C) |                   |                         |                            |
| 10%                  | 214.5             | 210.0                   | 209.2                      |
| 30                   | 248.0             | 239.5                   | 216.2                      |
| 50                   | 271.5             | 264.5                   | 224.9                      |
| 70                   | 297.5             | 299.0                   | 236.3                      |
| 90                   | 331.5             | 333.5                   | 255.0                      |
| End point            | 370.5             | 358.5                   | 280.4                      |

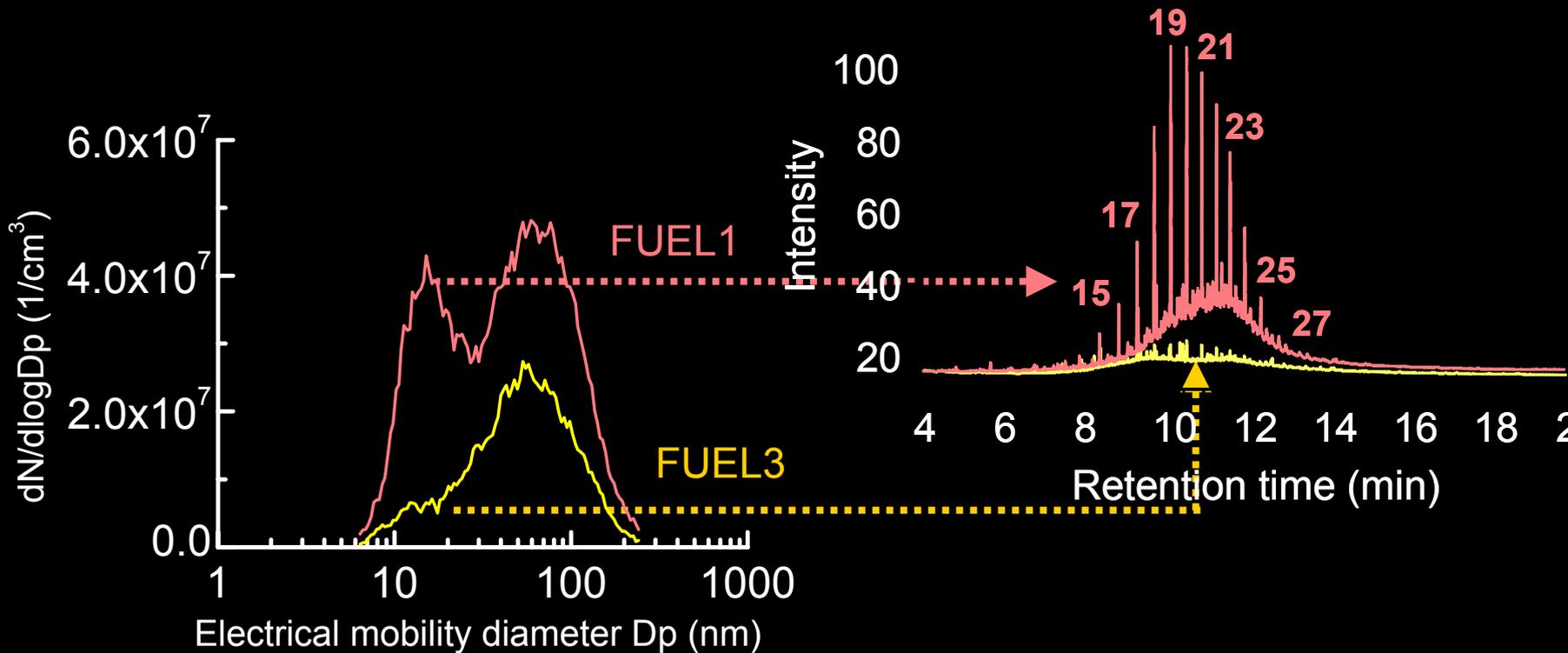
# Nucleation Particles at idle

750rpm-0Nm



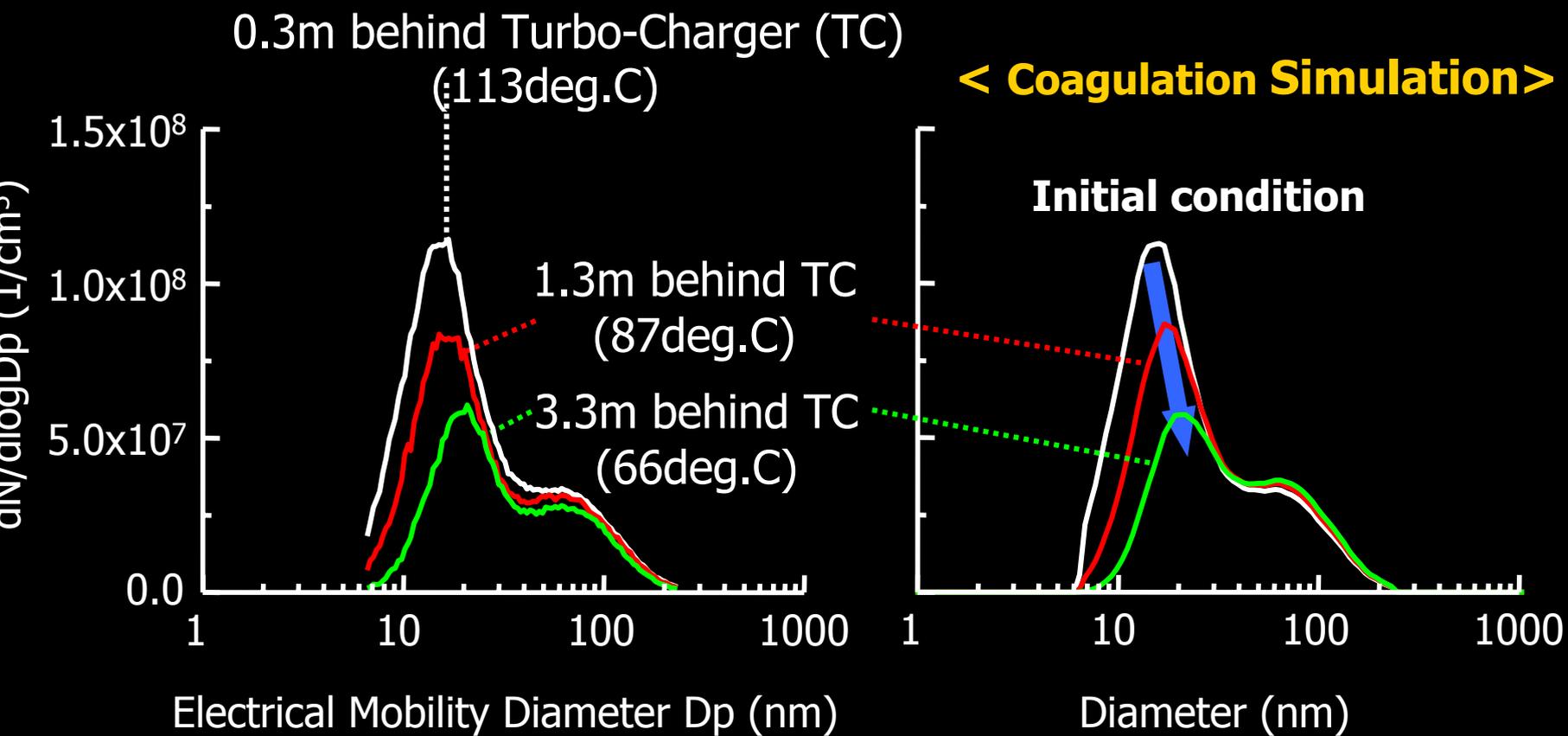
- Formation of nucleation particles at idle depends strongly on fuel property.

# Chromatogram of SOF



- More than C18 hydrocarbons in fuel are main components of nucleation particles at idle.

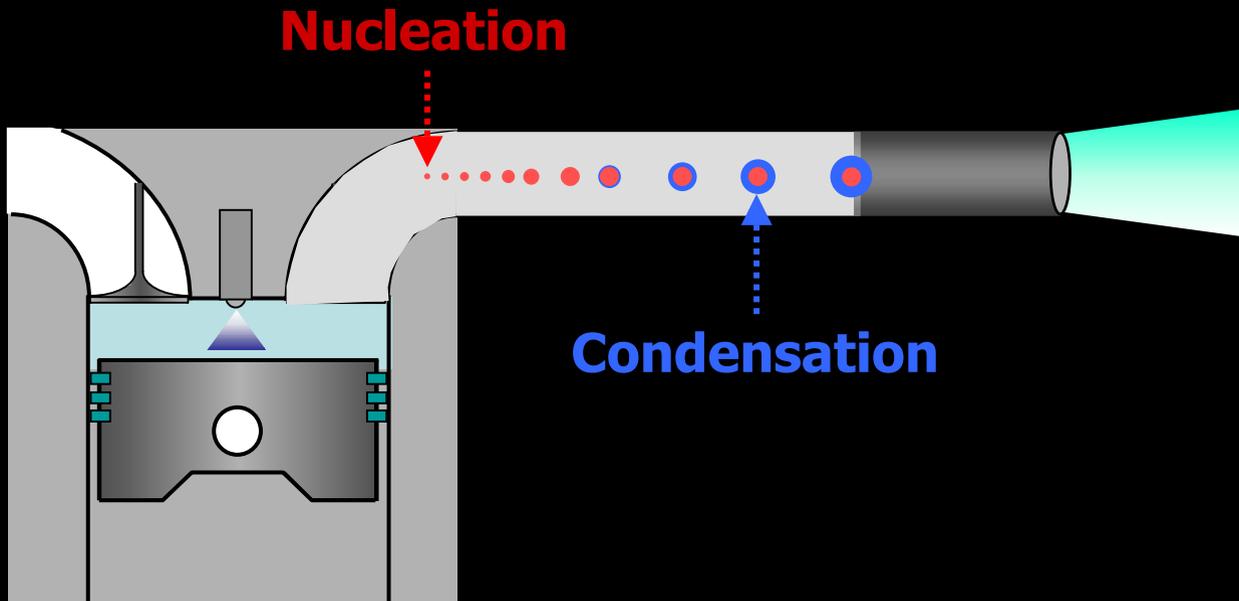
# Where are Nucleation Particles formed?



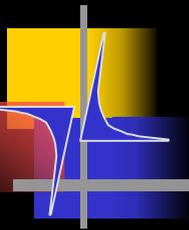
- Nucleation particles exist at exhaust gas temperature that exceeds 100 C in exhaust-pipe.

# Nucleation Particles at idle

- Nucleation particles exist at exhaust gas temperature that exceeds 100 C in exhaust-pipe.
- More than C18 hydrocarbons in fuel are main components of nucleation particles at idle.



## 2. Simulation of Nucleation Particles at Idle



$$\frac{\partial N_k}{\partial t} = \frac{1}{2} \sum_{j=1}^{k-1} \beta_{k-j,j} N_{k-j} N_j - N_k \sum_{j=1}^n \beta_{k,j} N_j$$

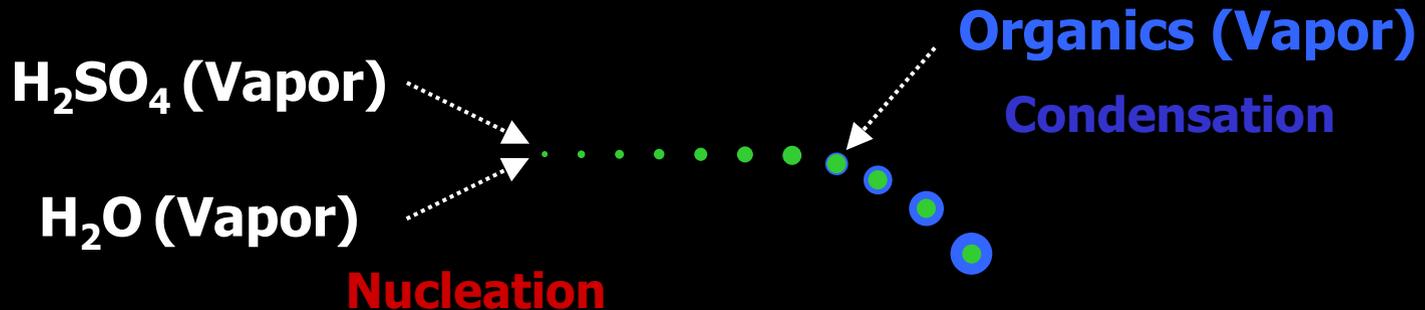
$$\frac{\partial m_k}{\partial t} = 2\pi D_i D_{pk} N_k f(Kn_k, \alpha) [C - C^{eq} \eta_k]$$

$$J = \left( \frac{2\sigma}{\pi m_1} \right)^{1/2} \frac{v_1 N_1^2}{S} \exp \left[ -\frac{16\pi}{3} \frac{v_1^2 \sigma^3}{(k_B T)^3 (\ln S)^2} \right]$$

# Nanoparticle formation Mechanisms

- Formation mechanism of nucleation particles at idle cannot be explained by BHN theory as nucleation particles form at exhaust gas temperature that exceeds 100 C in exhaust-pipe.

- Binary Homogeneous Nucleation (BHN) theory -



# Hydrocarbon Nucleation

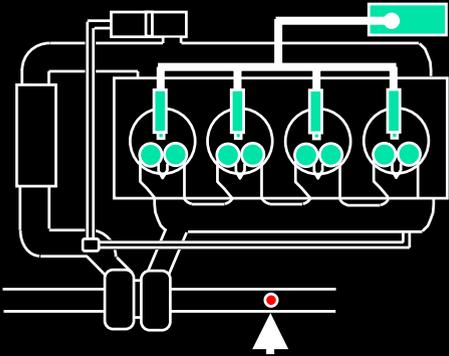
- We tried to simulate formation of nucleation particles at idle through hydrocarbon nucleation by following three fundamental equations.

Coagulation 
$$\frac{\partial N_k}{\partial t} = \frac{1}{2} \sum_{j=1}^{k-1} \beta_{k-j,j} N_{k-j} N_j - N_k \sum_{j=1}^n \beta_{k,j} N_j$$

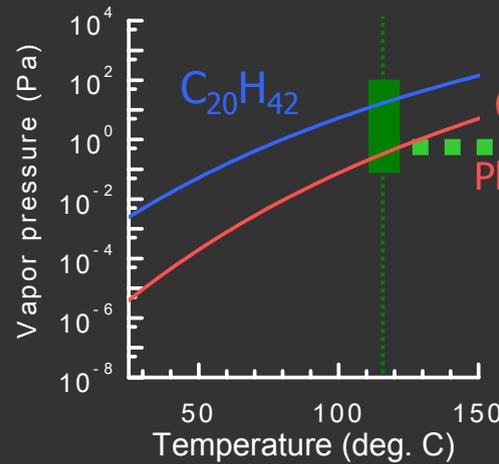
Condensation  
/Vaporization 
$$\frac{\partial m_k}{\partial t} = 2\pi D_i D_{pk} N_k f(Kn_k, \alpha) [C - C^{eq} \eta_k]$$

Nucleation 
$$J = \left( \frac{2\sigma}{\pi m_1} \right)^{1/2} \frac{v_1 N_1^2}{S} \exp \left[ -\frac{16\pi}{3} \frac{v_1^2 \sigma^3}{(k_B T)^3 (\ln S)^2} \right]$$

# Nanoparticle Formation at Idle

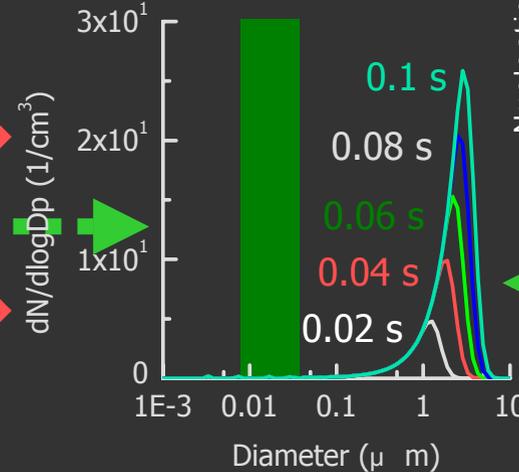
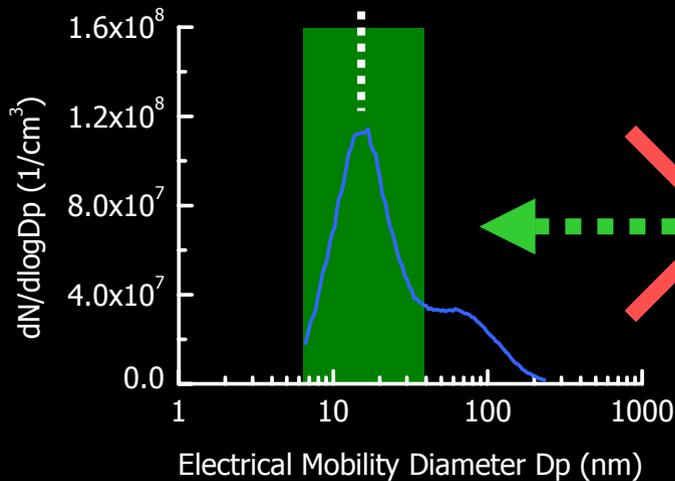
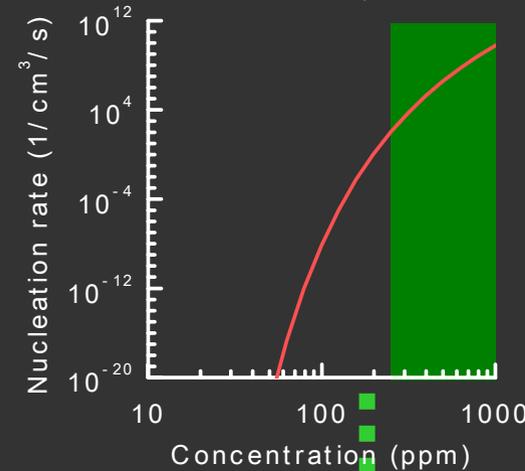


Exhaust gas Temp. = 113C



- Simulation -

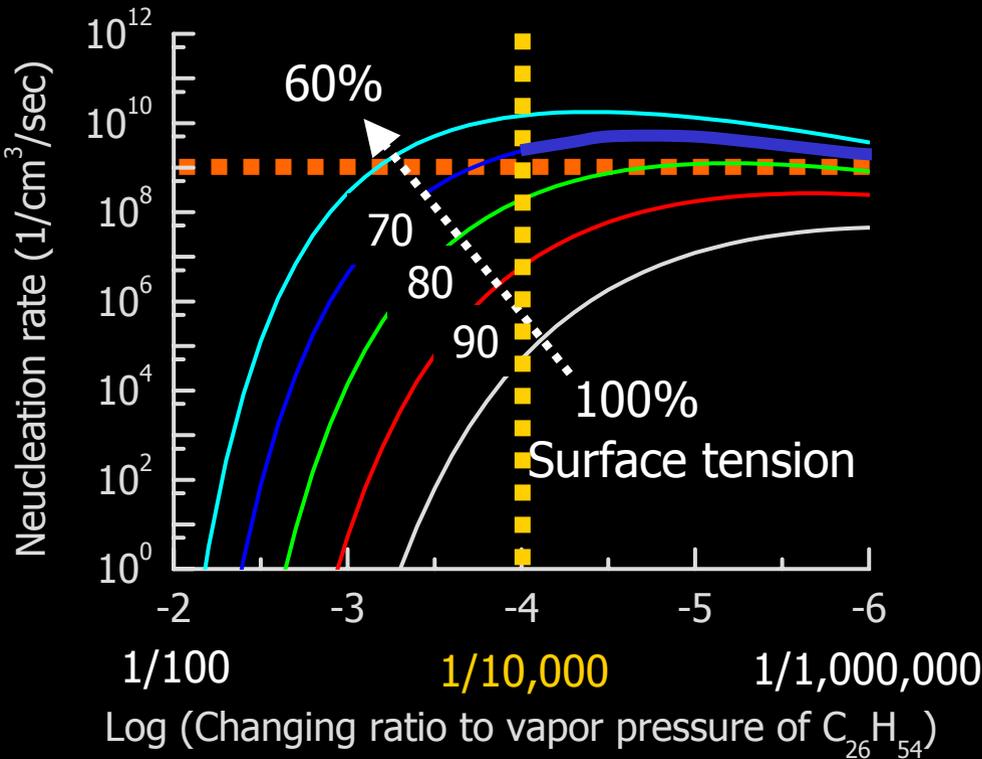
Physical properties of  $C_{26}H_{54}$  at 113 C



$C_{26}H_{54}$  = 250ppm  
Exhaust gas temp. = 113 deg.C

This result suggests the existence of other nucleation materials

# Nucleation Rate



/ Temperature: 113 deg. C  
 ,that is exhaust gas temp at idle.  
 / Concentration: 0.25 ppm

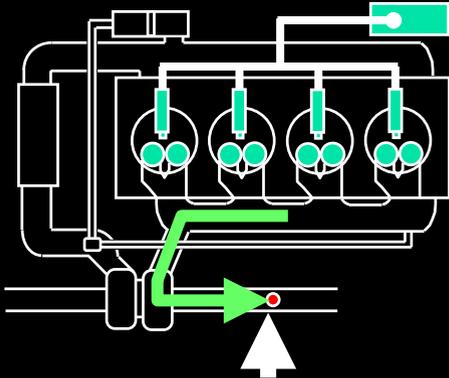
Effect of vapor pressure and surface tension on nucleation rate.

Nucleation rate needs  $10^9$  to get more than  $10^8$  part/ $\text{cm}^3$  nanoparticles at idle.

- Considering 1/10,000 in vapor pressure and 70% in surface tension to those of  $\text{C}_{26}\text{H}_{54}$ , we can simulate enough nucleation rate.

# Simulation of Nanoparticle Formation

750rpm-0Nm (idle)

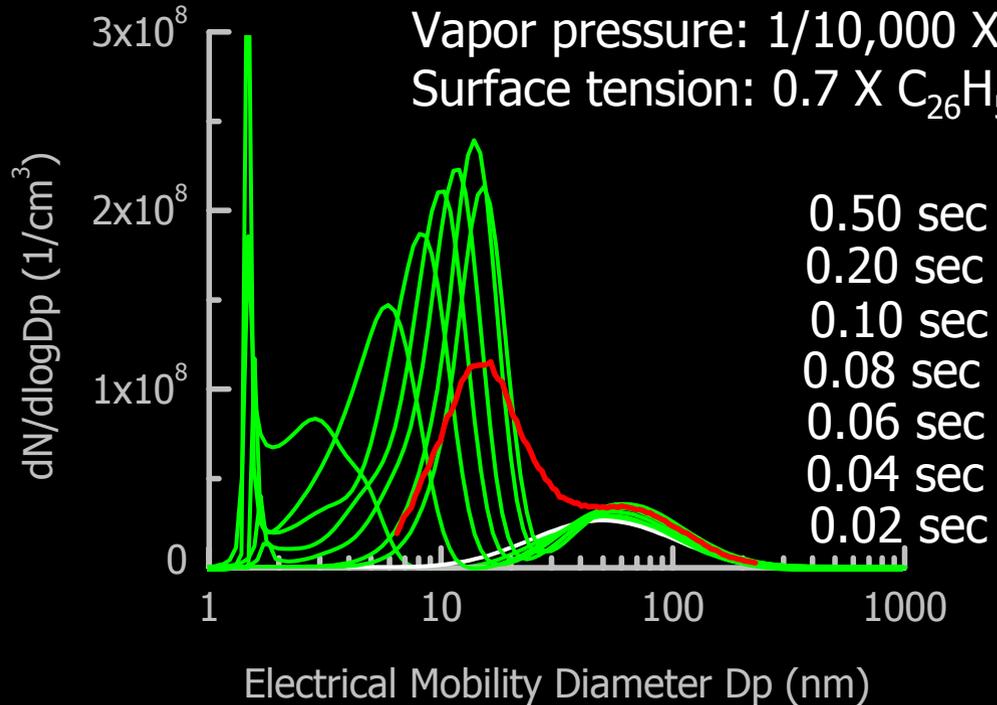


Exhaust gas Temp.=113C

< Initial value >

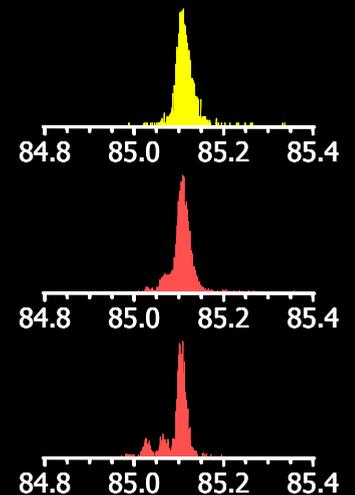
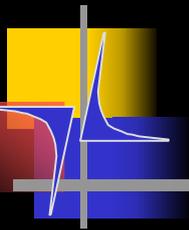
at Idle

- Soot maximum conc.:  $2E+7$  part./ $cm^3$   
with log-normal shape
- Nucleation material (NM) : 0.25ppm  
Vapor pressure:  $1/10,000 \times C_{26}H_{54}$   
Surface tension:  $0.7 \times C_{26}H_{54}$



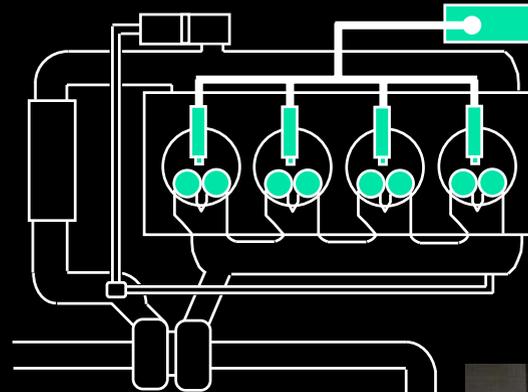
- Considering specific physical properties of NM, simulation result is in good agreement with experimental result.

# 3. Chemical Analysis of Nucleation Particles at idle



# Experimental Set-up

- Engine operating condition : 750rpm-0Nm
- Fuel : **S=420ppm** diesel fuel



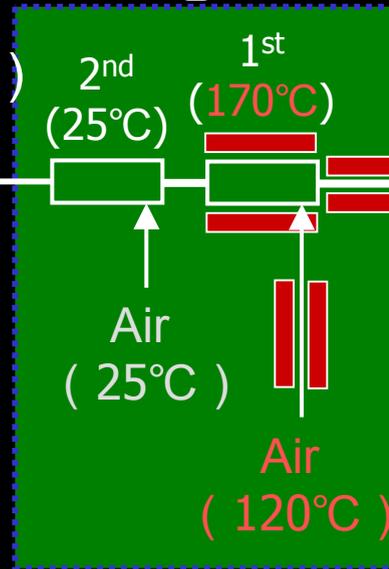
4-cylinder (2L)  
DI diesel engine

DEKATI Dilutor  
( Dilution ratio: 64 )

30L/min



SMPS

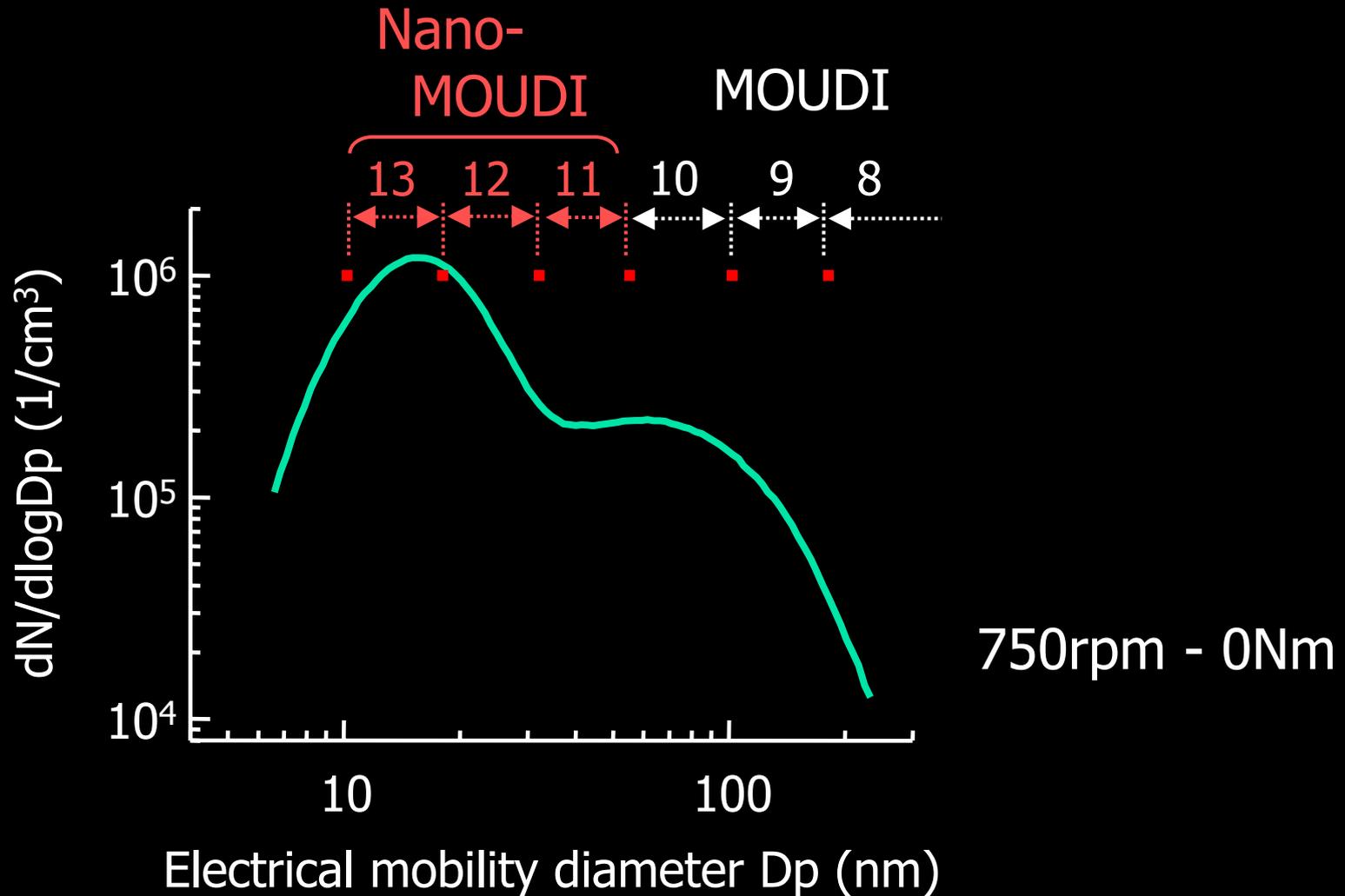


Sampling period : 5 hours

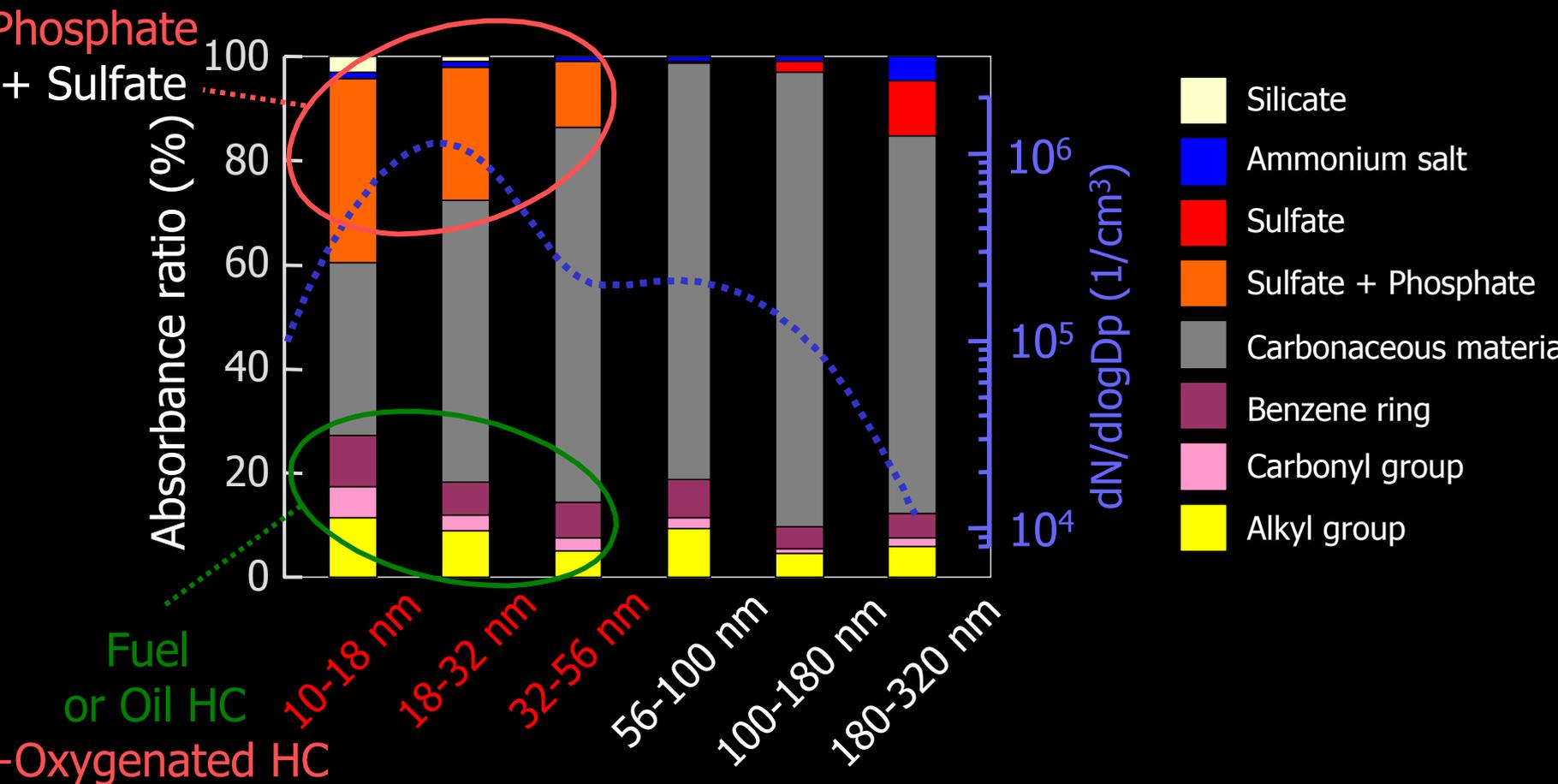


\* SMPS: Scanning Mobility Particle Sizer

# Classified Particle Diameter Ranges



# FT-IR Analysis of Classified Particles



- Phosphate and oxygenated HCs are detected mainly in the range of 10-56nm in diameter.

# TOF-SIMS Analysis for Heterocompounds

Fragment signal of heterocompounds

Fragment signal of aliphatic hydrocarbons

Engine oil

84.8 85.0 85.2 85.4 m/z

100-180nm

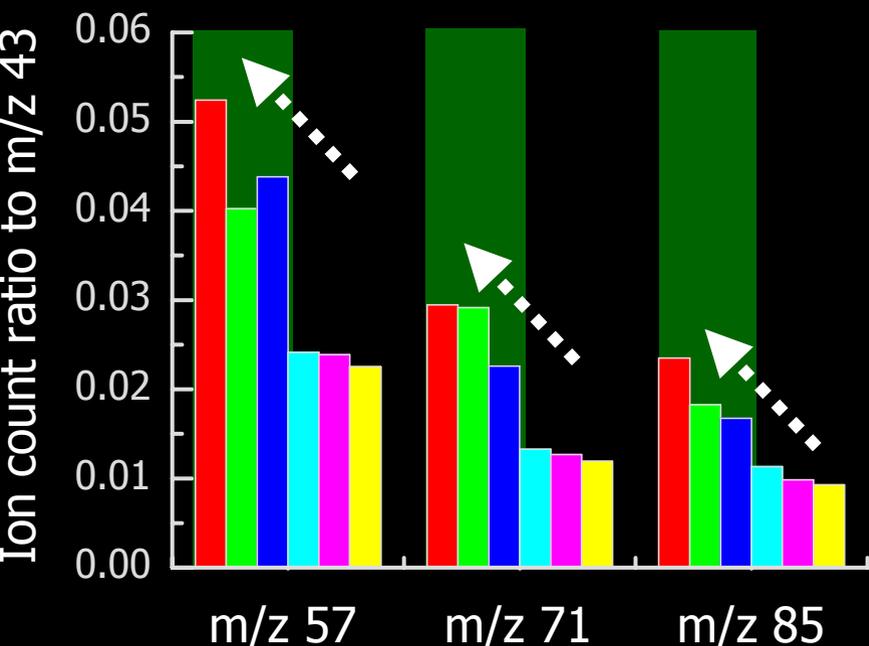
84.8 85.0 85.2 85.4 m/z

10-18nm

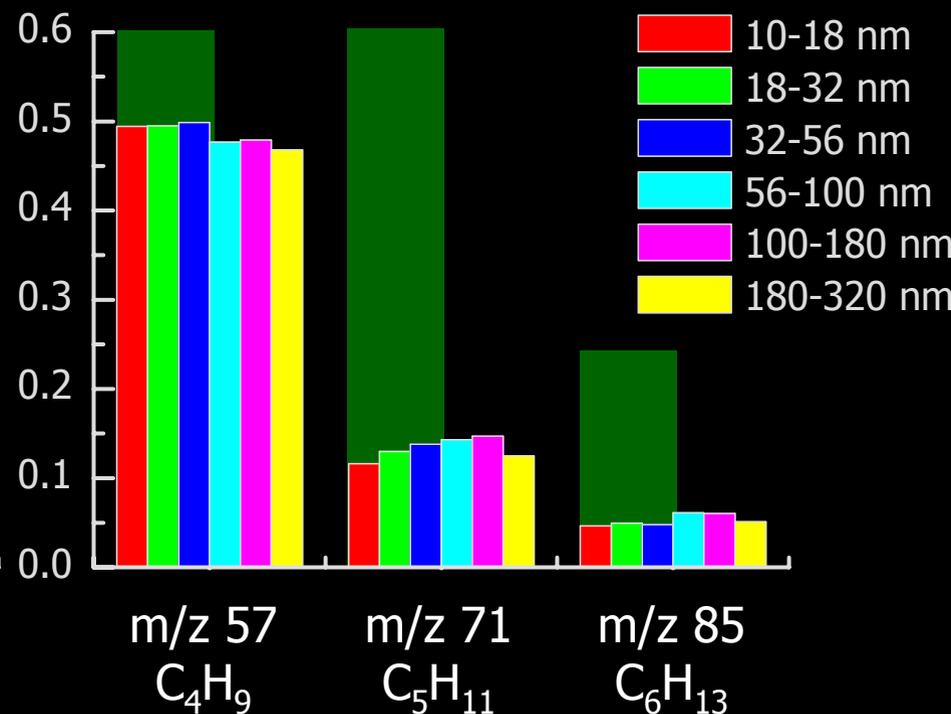
84.8 85.0 85.2 85.4 m/z

# Heterocompounds in Nucleation particles

## <Heterocompounds, C-H-O>

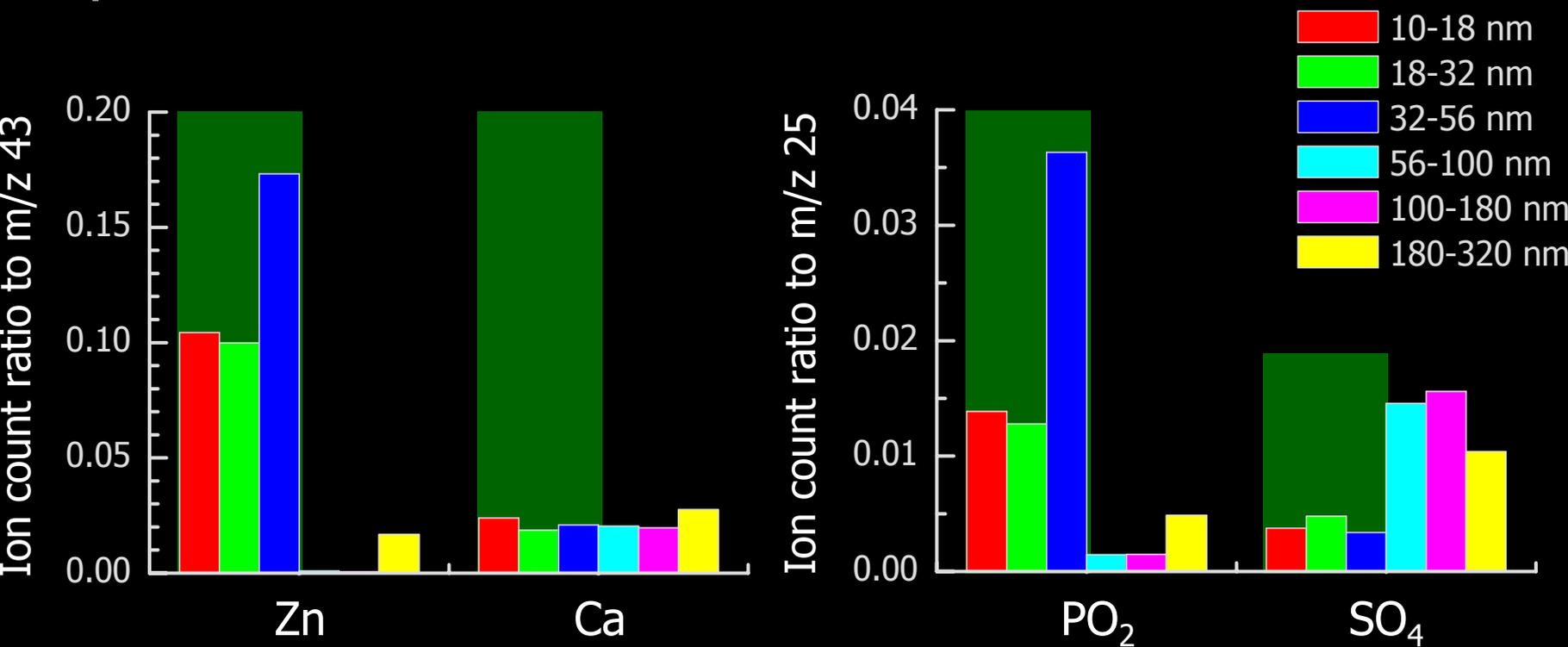


## <Aliphatic hydrocarbons, C-H>



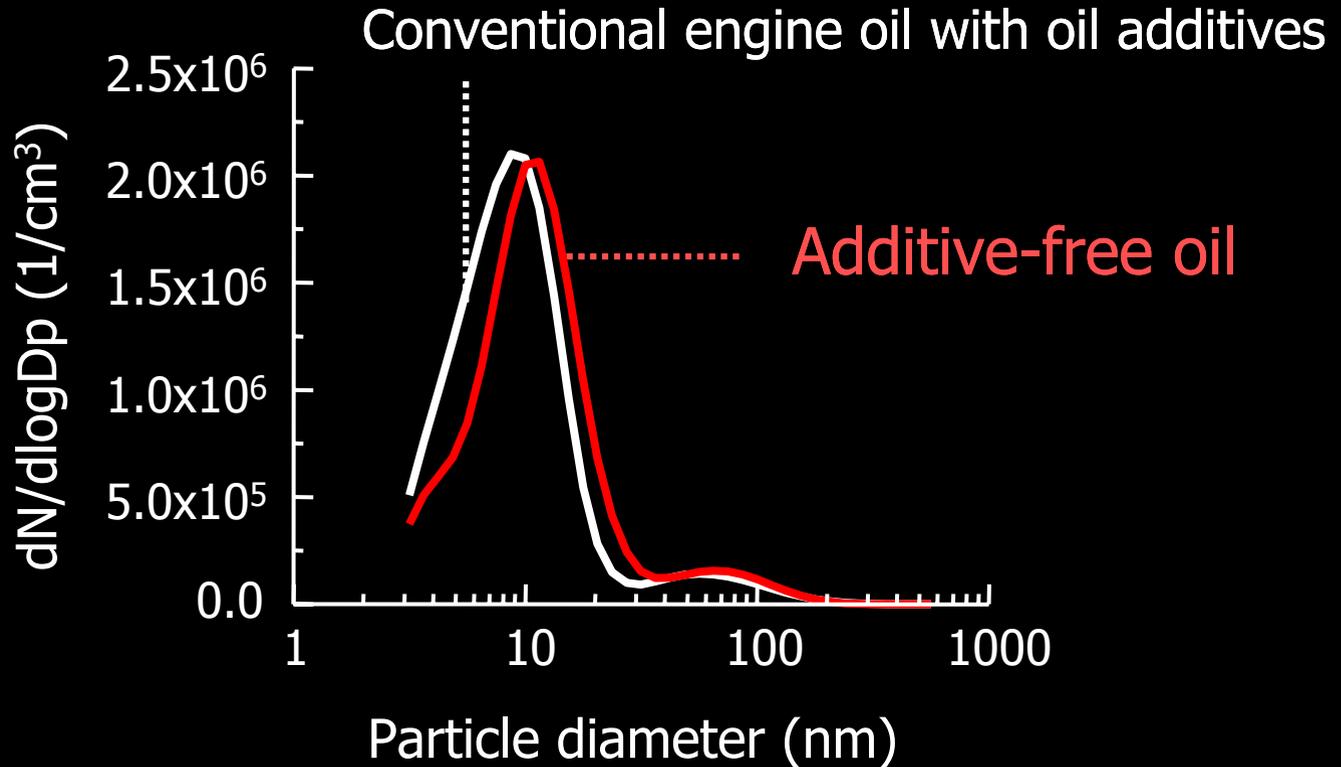
- Percentage content of hetero-compound increases in the range of nanoparticle diameter.

# Effect of Inorganic Compounds

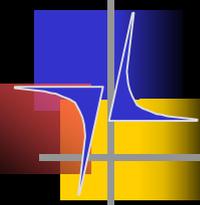


- Percentage contents of **Zn** and  **$PO_2$**  increase in the range of nanoparticle diameter.
- Zn and  $PO_2$  would be pyrolytic products of oil additive (**Zn-DTP**).

# Nucleation at Idle and Oil Additives



- Oil additives do not contribute to nucleation of nanoparticles at idle.



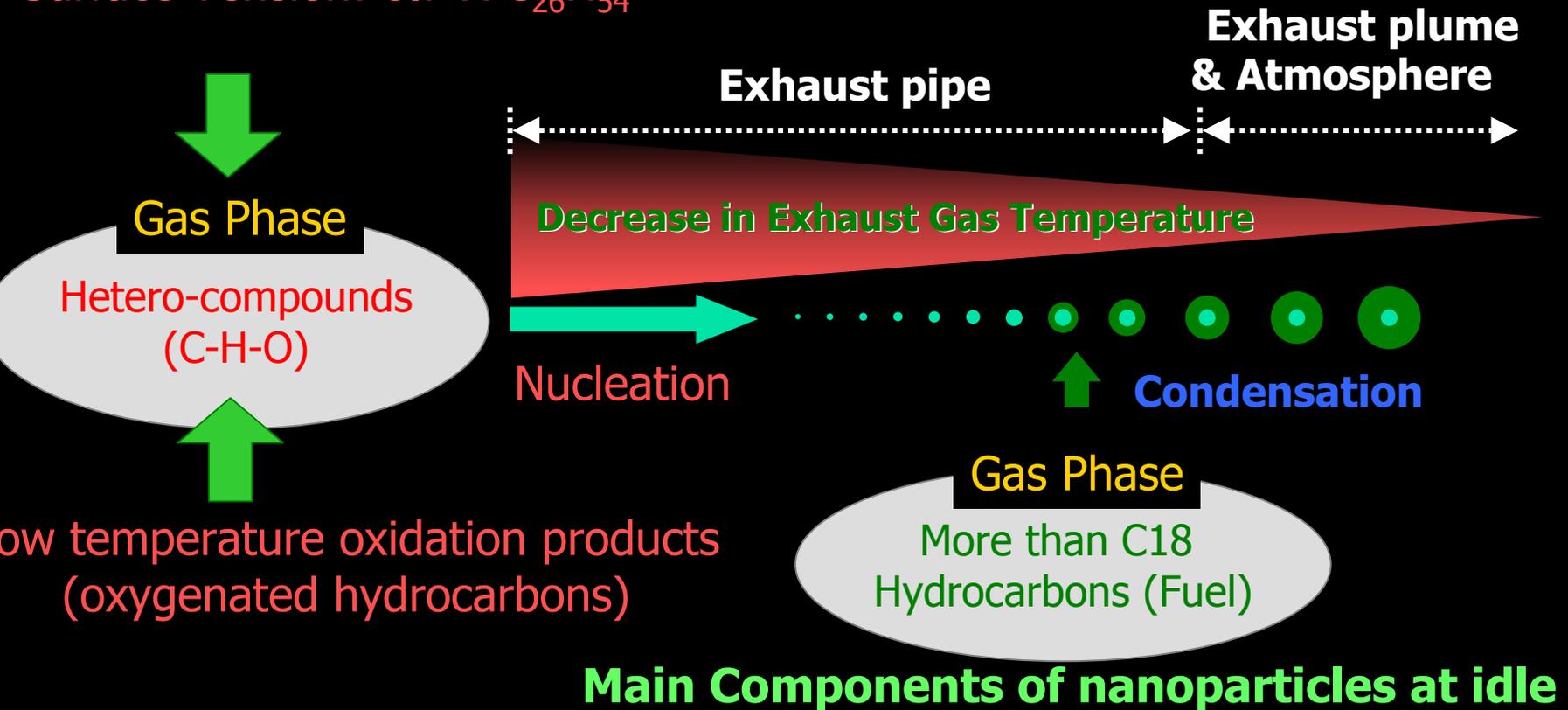
# Analysis of Nucleation Particles at Idle

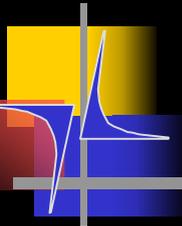
We analyzed nucleation particles to clarify some nucleation materials in the formation of nucleation particles at idle.

- Hydrocarbons of fuel or oil are observed in the whole diameter range and its percentage contents are independent of particle diameter.
- Hetero-compounds (low temperature oxidation HCs) exist in a high ratio in the range of nanoparticle diameter.
- These compounds have lower vapor pressure than high boiling point HCs in fuel ( $C_{26}H_{54}$ ) have.
- Hetero-compounds would be nucleation material under idling condition.

# Formation Mechanism of Nucleation Particles under Idling Condition

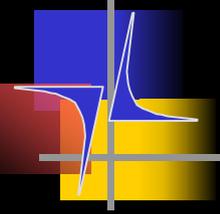
Vapor Pressure:  $1/10,000 \times C_{26}H_{54}$   
Surface Tension:  $0.7 \times C_{26}H_{54}$





*Thank you very much  
for your attention!!*

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# GC-MS Analysis of Classified Particles 1

$\langle m/z=85 \rangle$

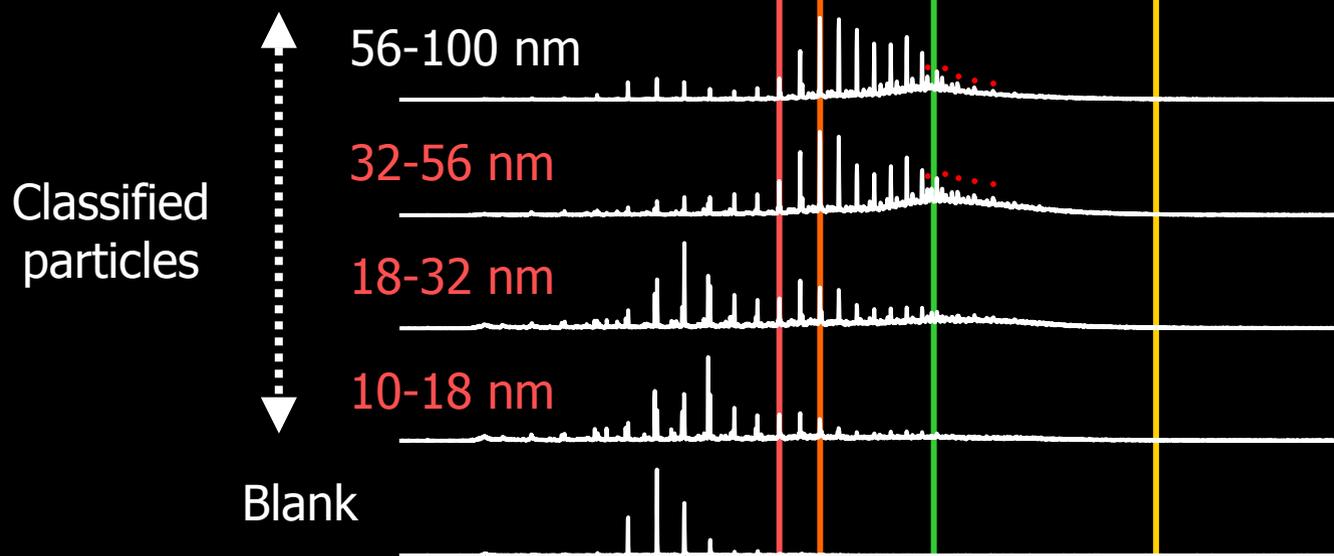
Elution peak of fuel elements

Beginning of elution of fuel elements

Elution peak of oil elements

End point of elution of oil elements

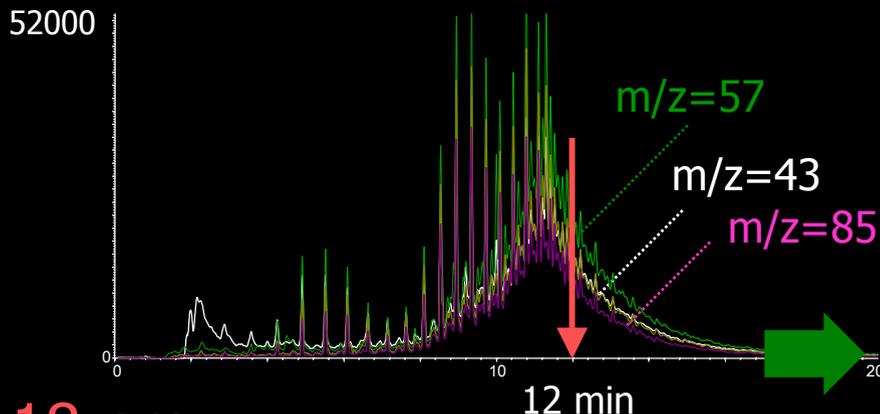
Mixture of high boiling point elements in fuel, and oil



- Elements of fuel and oil exist in a whole range of particle diameter.

# Comparison between m/z85 and m/z43

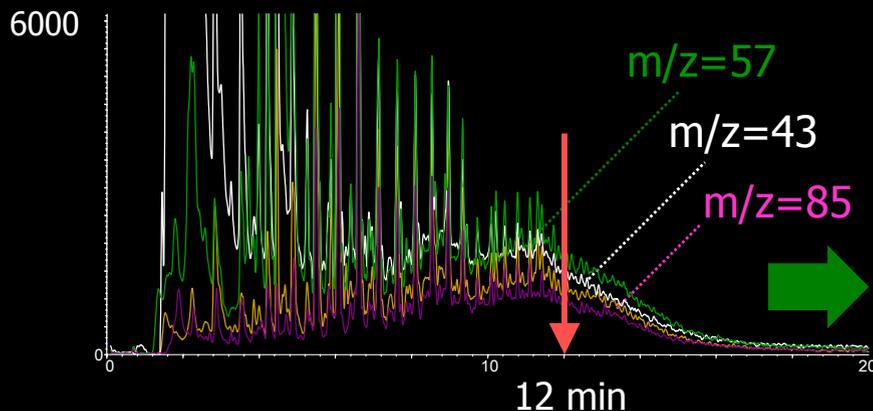
56-100 nm



Mixture of high boiling point elements in fuel, and oil

$$\frac{(m/z=85)}{(m/z=43)} = 0.82 \text{ (12 min)}$$

10-18 nm

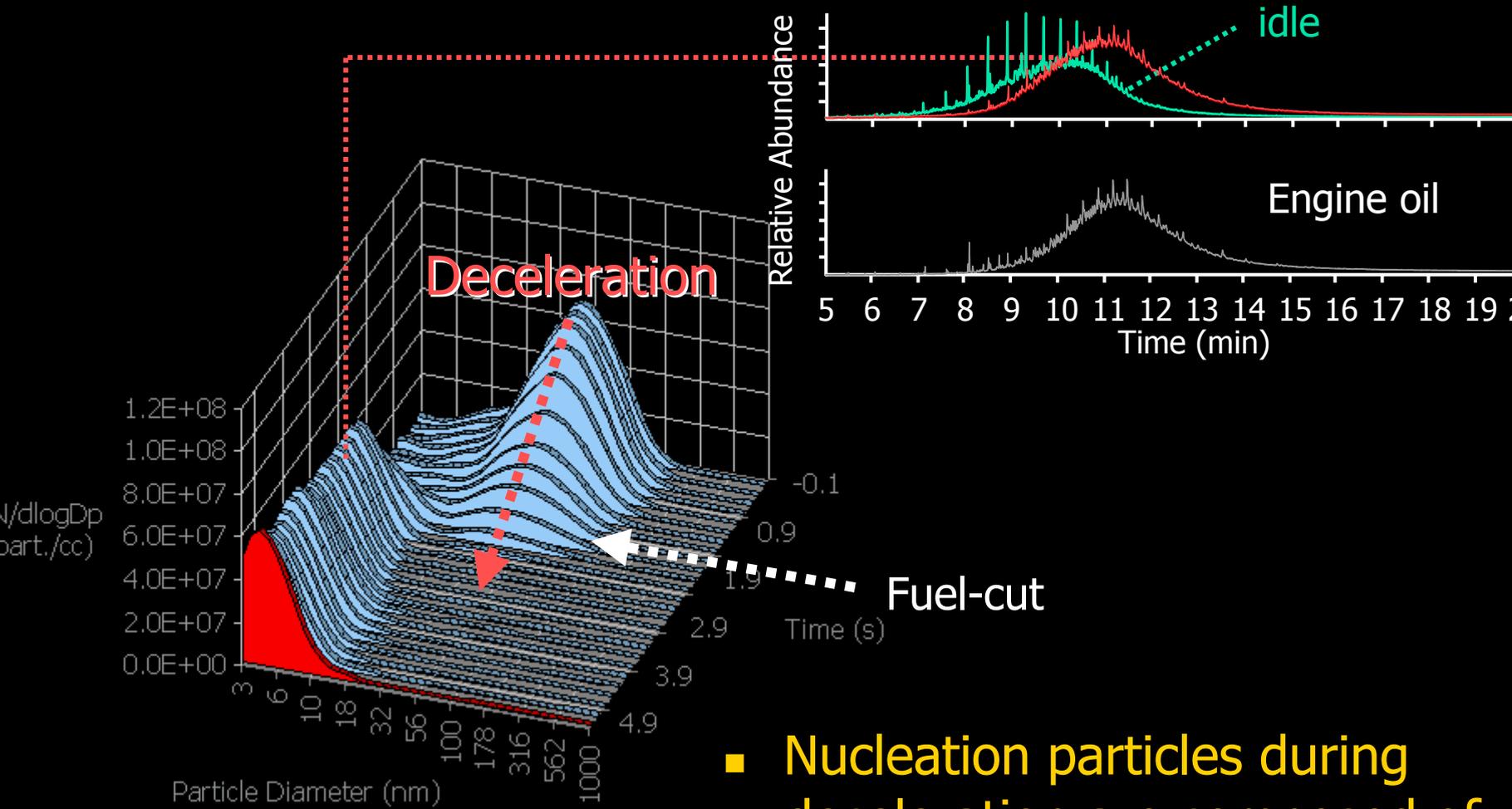


$$\frac{(m/z=85)}{(m/z=43)} = 0.70 \text{ (12 min)}$$

$$\frac{(m/z=85)}{(m/z=43)} = 0.57 \text{ (12 min)}$$

- This result suggests existence of heterocompounds (C-H-O) in the range of nanoparticle diameter.

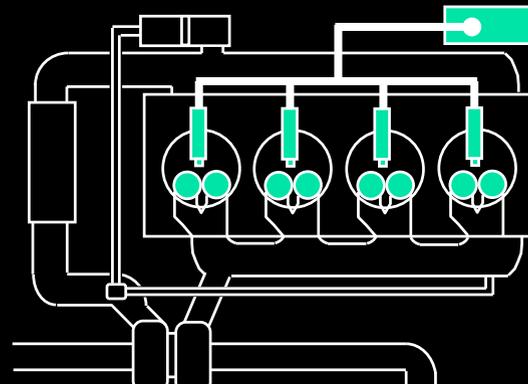
# Nucleation particles during Deceleration



- Nucleation particles during deceleration are composed of engine oil elements.

# Experimental Set-up for Transient Test

- Engine operating condition :  
2500rpm-110Nm  
-> 2500rpm-Motoring
- Fuel : S=420ppm diesel fuel



4-cylinder (2L)  
DI diesel engine

DEKATI Dilutor  
( Dilution ratio: 64 )

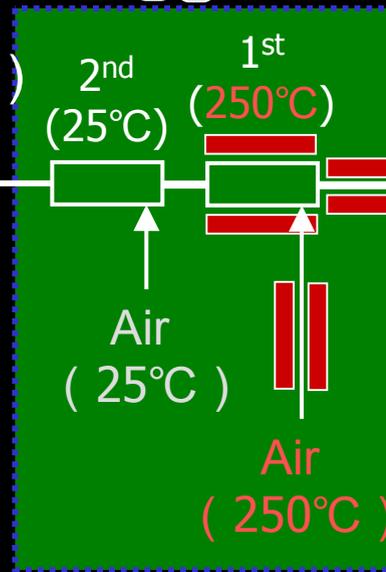
**DMS500**  
Fast Particulate Spectrometer

CAMBUSTION

A Differential Mobility Spectrometer for real time measurement of exhaust particulate size spectra

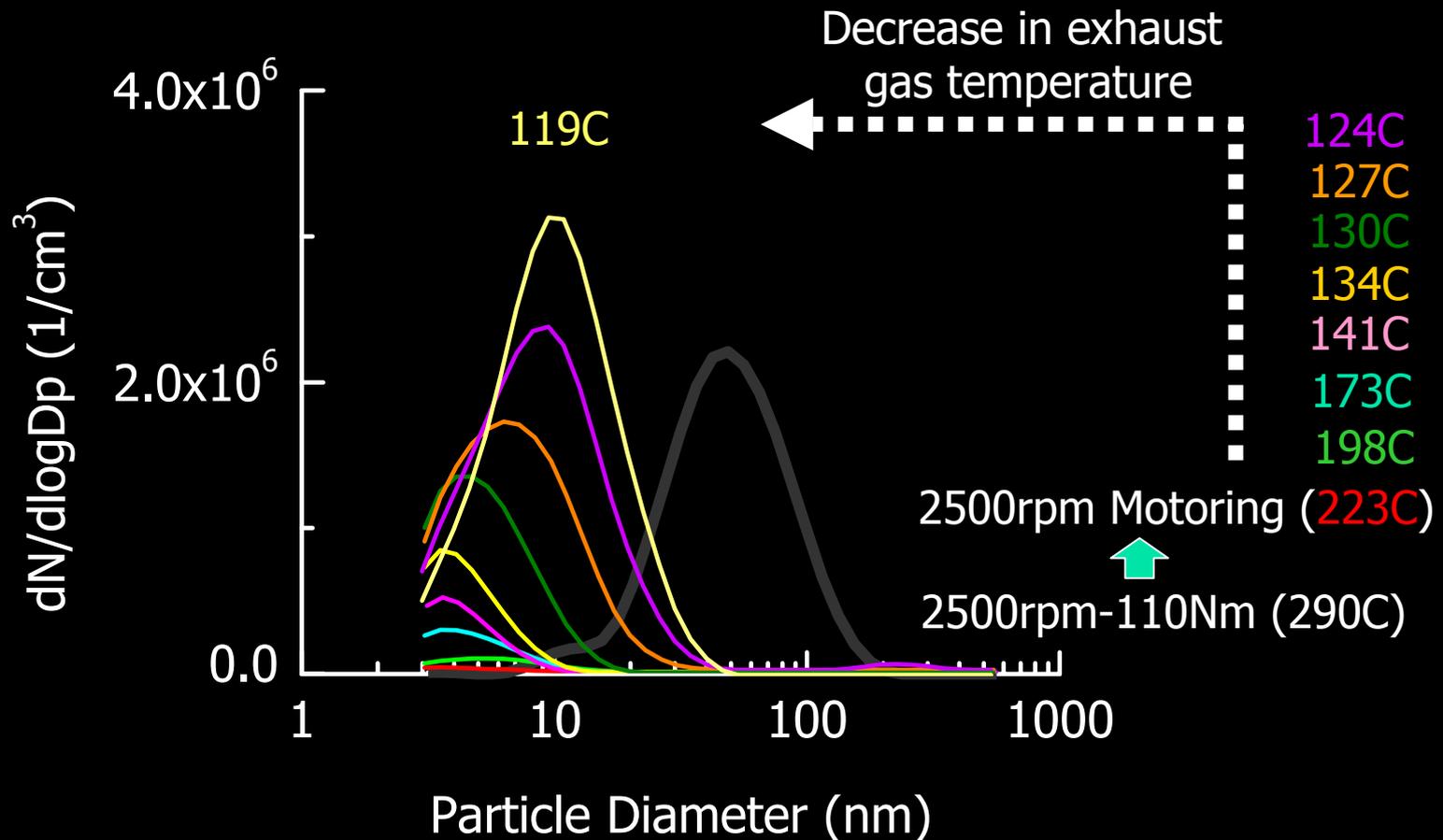
DMS500 (Diluted Diesel) Exhaust Particulate Spectrometer

- Fast response (complete spectrum in 200ms)
- Size range of 5nm to 1,000nm
- Spectrum output at 16 sizes per decade
- Continuous output of total mass and number



Measurement of  
exhaust gas temperature

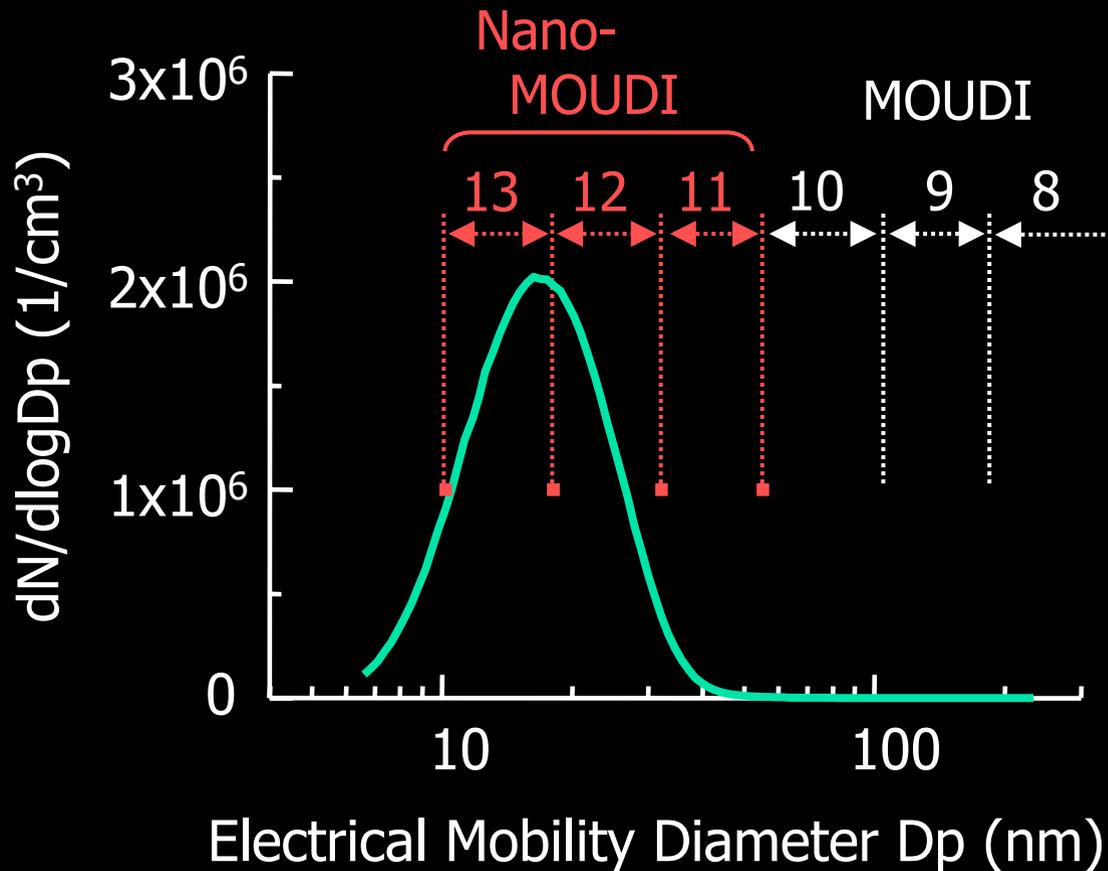
# Formation of Nucleation Particles under deceleration condition



- Nucleation particles under deceleration condition also exist at more than 100 C of exhaust gas temperature.

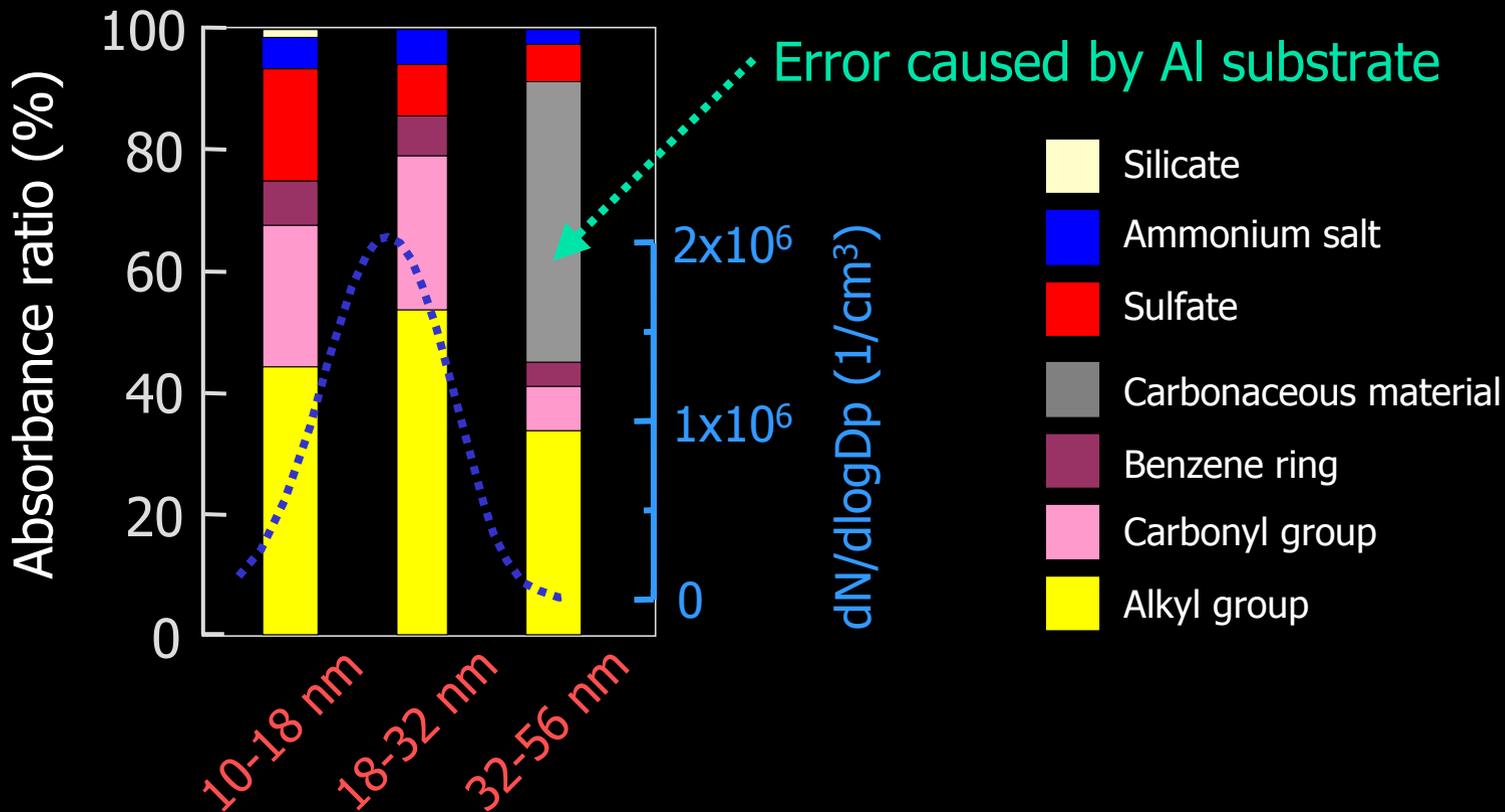
# Particle Size Distribution during Motoring

1250rpm



# FT-IR Analysis of Nucleation Particles

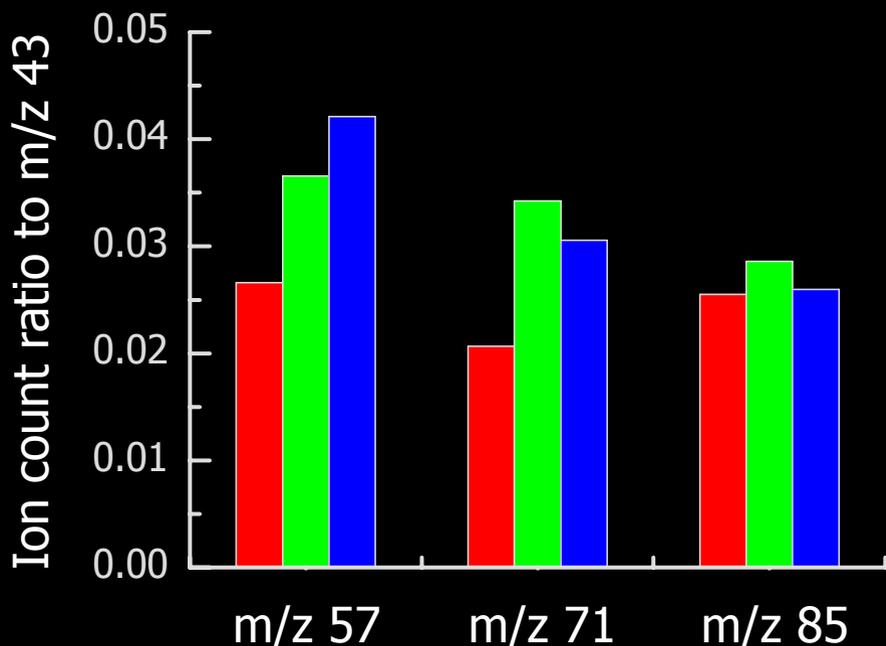
Under Motoring Condition



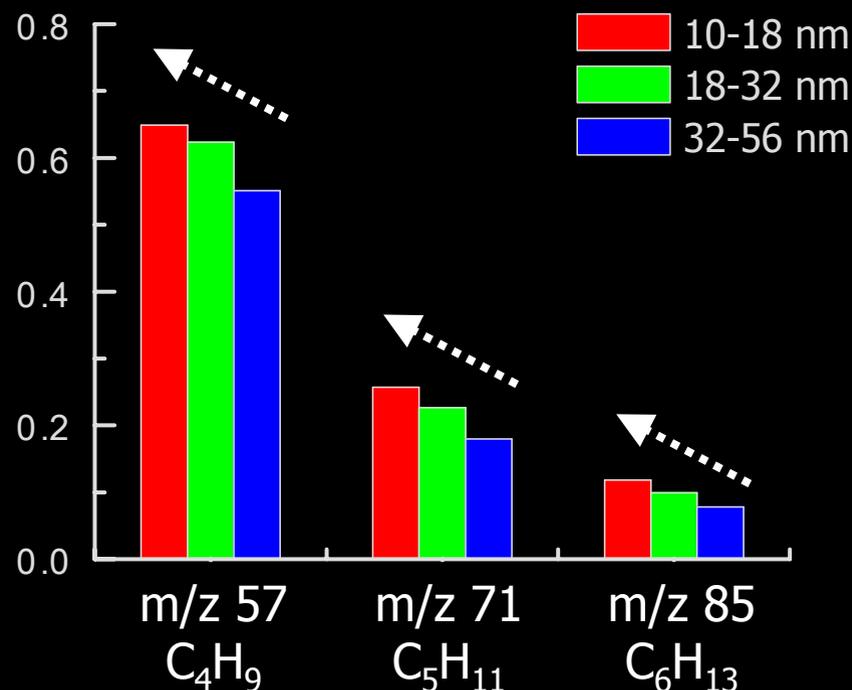
- Hydrocarbons and oxygenated hydrocarbons are the main components of nucleation particles under motoring condition.

# Nucleation Materials under Motoring 1

<Heterocompounds, C-H-O>



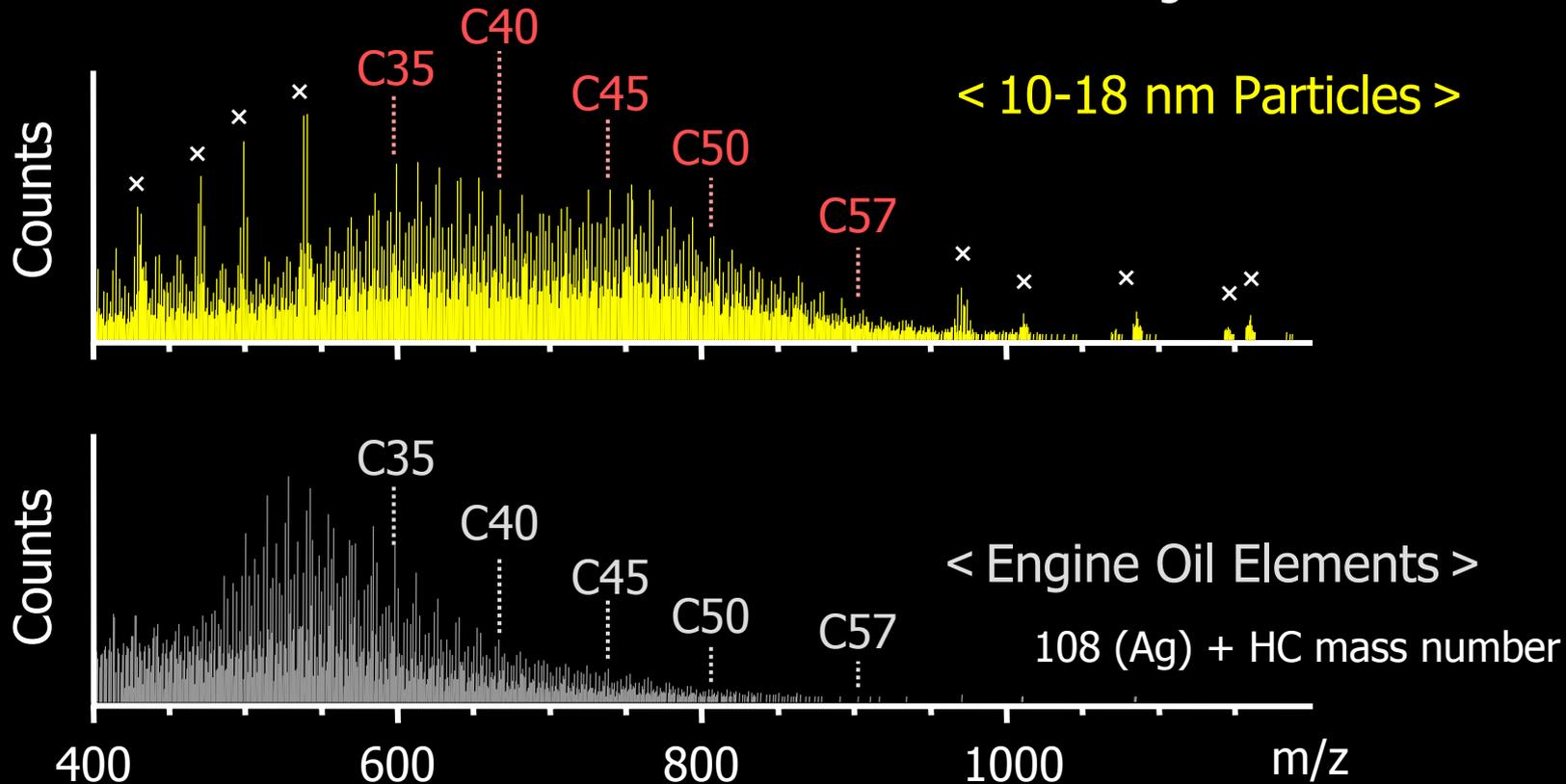
<Aliphatic hydrocarbons, C-H>



- The percentage content of aliphatic hydrocarbons increases with decrease in particle diameter in contrast to that of the hetero-compounds.

# Nucleation Materials under Motoring 2

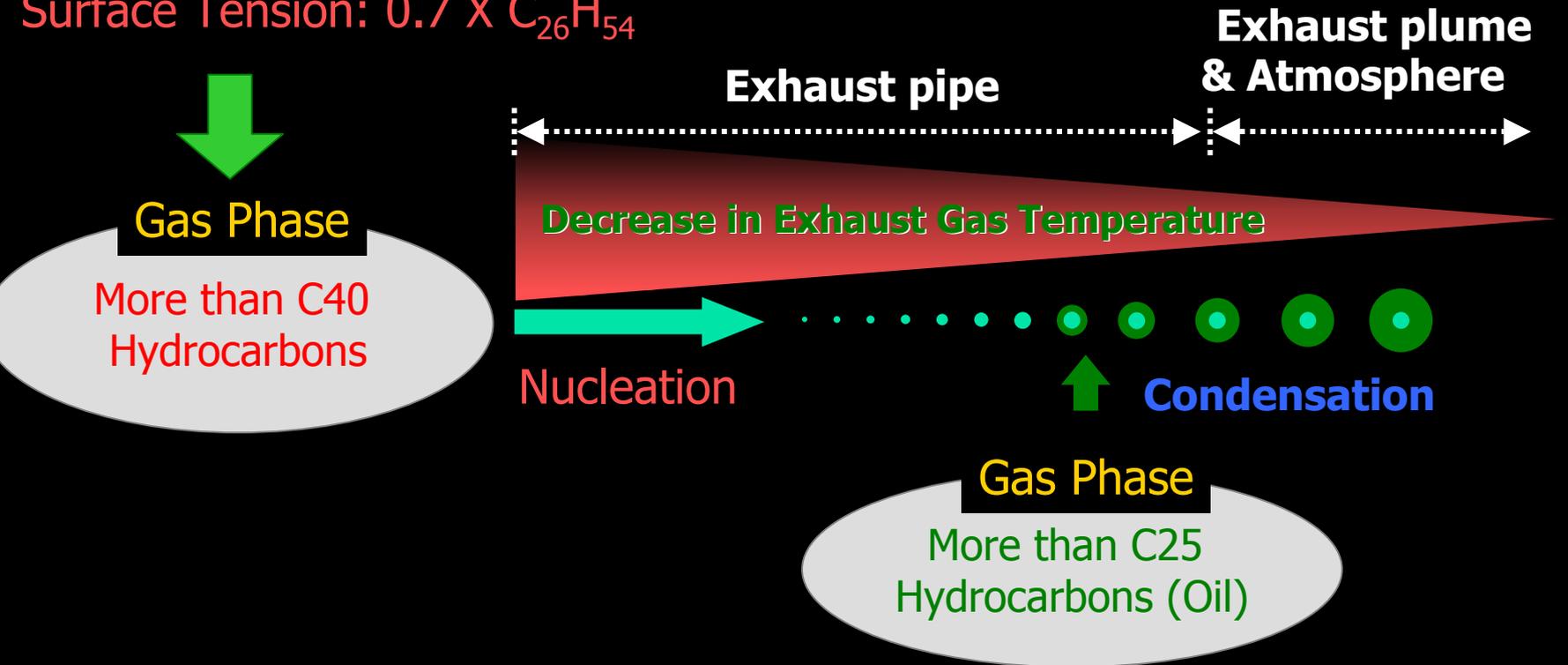
TOF-SIMS with Ag-Enhanced Method



- More than C40 paraffins of oil elements would be nucleation material under motoring condition ( under deceleration condition).

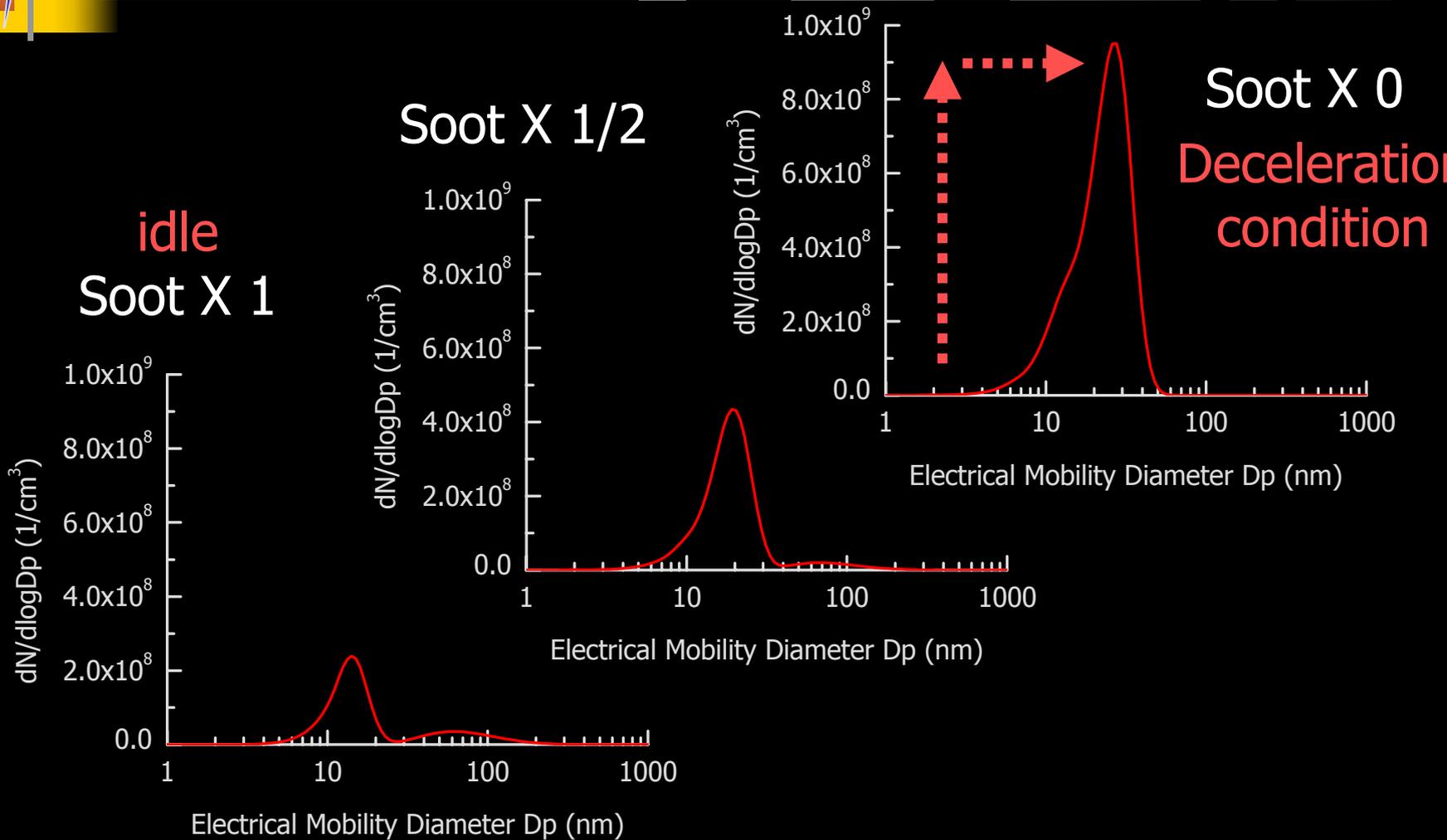
# Formation Mechanism of Nucleation Particles under Deceleration Condition

Vapor Pressure:  $1/10,000 \times C_{26}H_{54}$   
Surface Tension:  $0.7 \times C_{26}H_{54}$



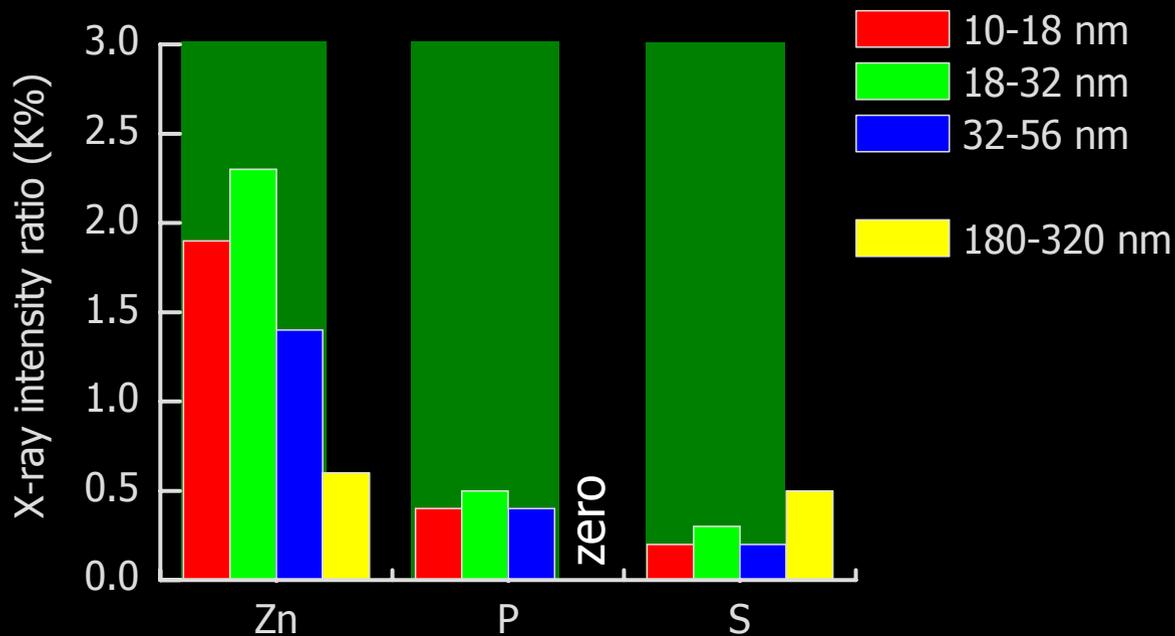
**Main Components of nucleation particles under deceleration condition**

# Effect of Soot Number Concentration



■ Suppression of soot causes increase in number concentration and diameter of volatile nanoparticles.

# EPMA Analysis of Classified particles



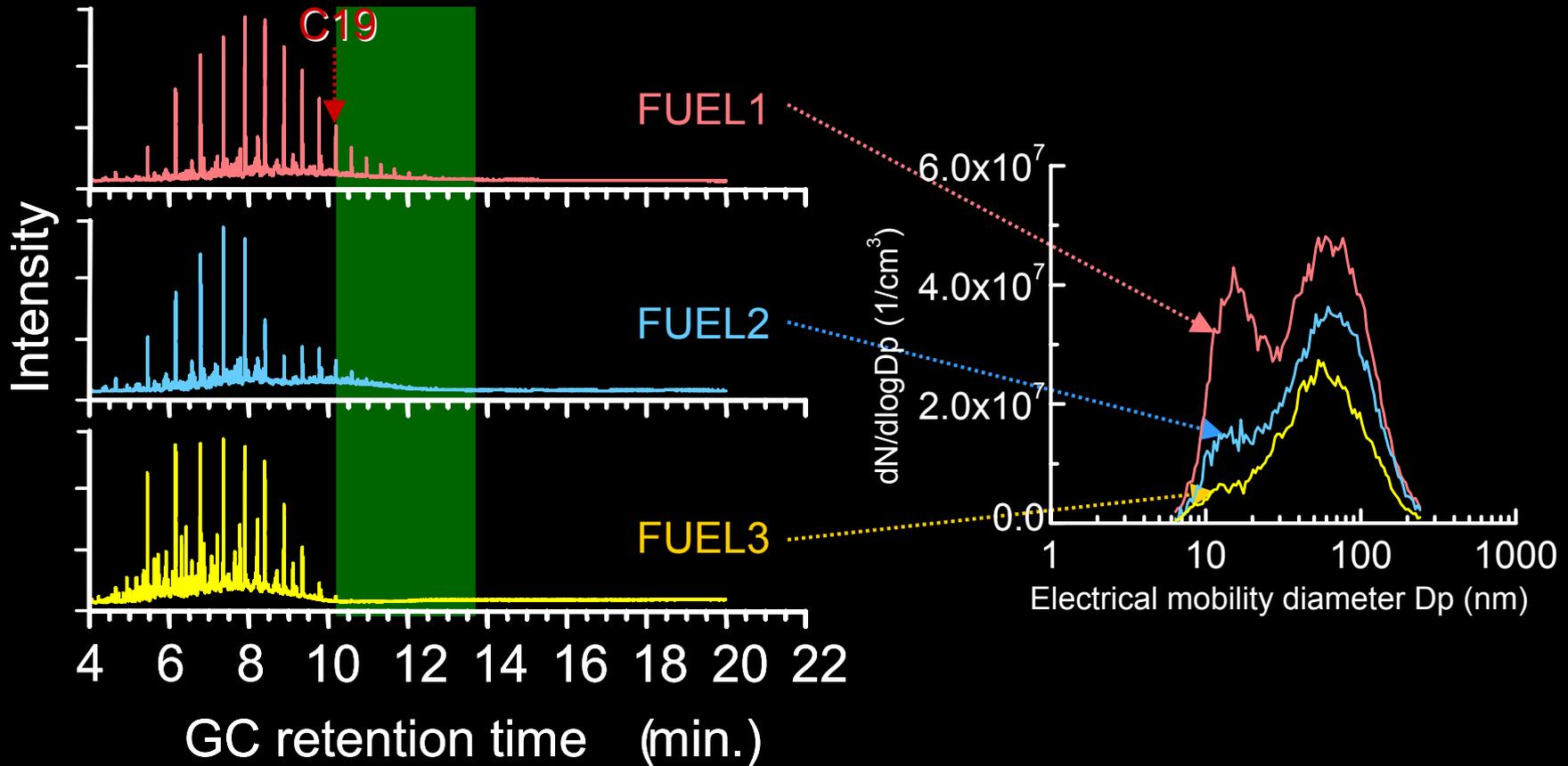
- Zn and P increase in the range of nanoparticle diameter
- EPMA data is in good agreement with TOF-SIMS data.

# Introduction

We clarified three engine operating conditions where volatile nanoparticles were observed and main components of volatile nanoparticles exhausted from a light-duty diesel engine system.

| Engine Operating Conditions | Idle (non-load)   | Deceleration  | Mid- & Hi-load  |
|-----------------------------|---|---|---|
| Main Components             | > C <sub>18</sub> HCs   | > C <sub>25</sub> HCs   | H <sub>2</sub> SO <sub>4</sub>  |
| Source                      | Fuel  | Oil   | Sulfur compounds in fuel  |
|                             |  |  |  |

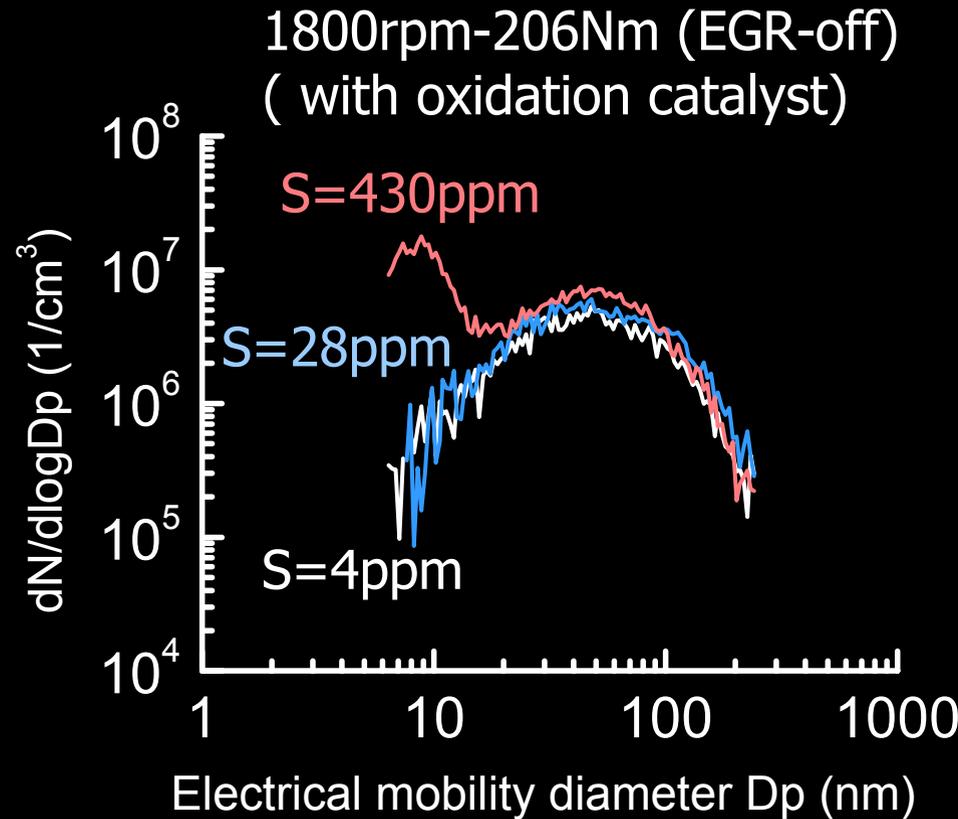
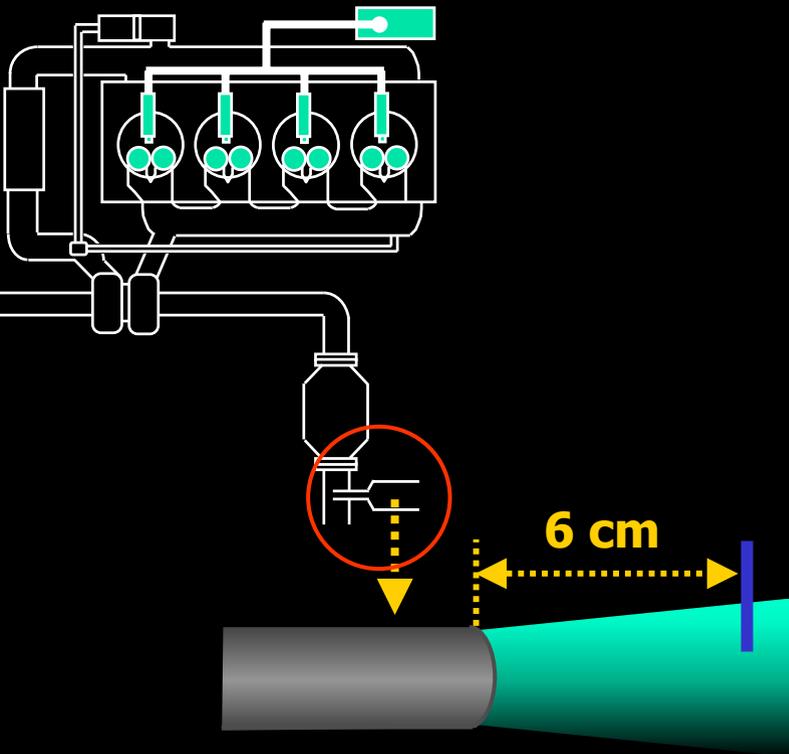
# Nanoparticles at idle



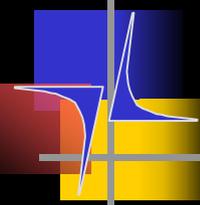
- Nanoparticles at idle are composed of more than C18 hydrocarbons in fuel.



# Nanoparticles under High Load Conditions



- Number concentration of nanoparticles depends on sulfur content in fuel. Nanoparticles under high load conditions consist of  $\text{H}_2\text{SO}_4$  formed by  $\text{SO}_3 + n\text{H}_2\text{O}$ .



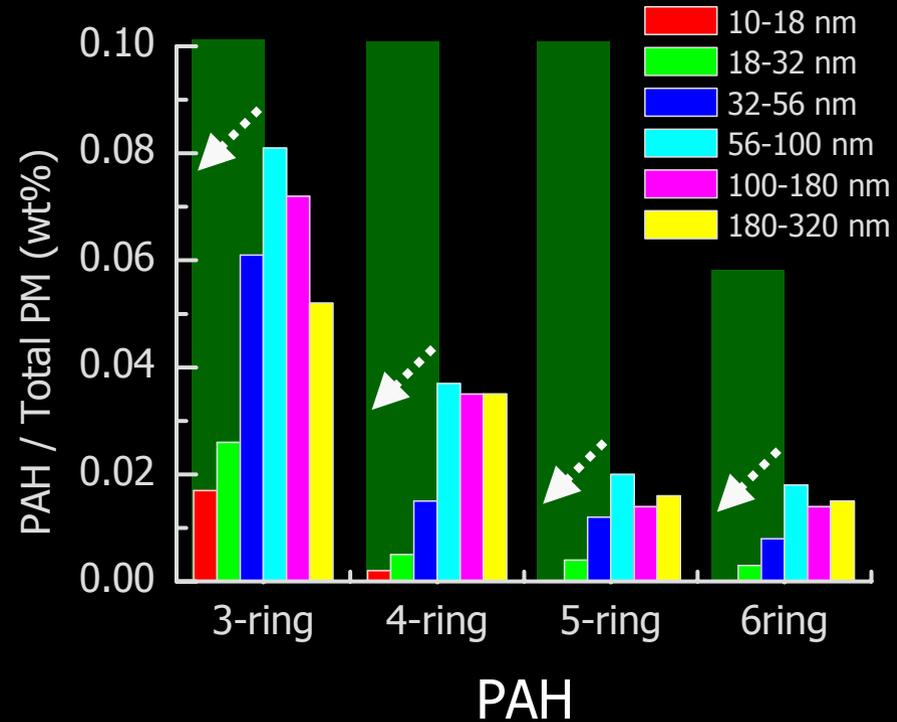
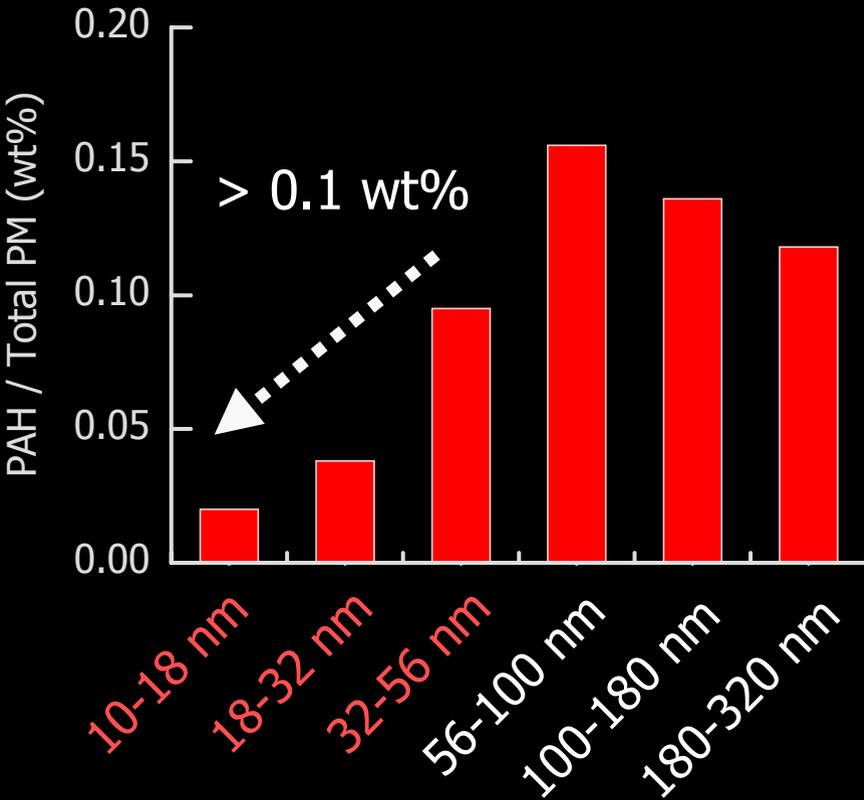
# Objective & Method

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- To clarify some nucleation materials in formation of volatile nanoparticles at idle.
  1. Particle sampling by using MOUDI & nano-MOUDL.
  2. Analysis of classified particles (10nm-320nm) with EPMA, FT-IR, GC-MS and TOF-SIMS.

# PAH Contents in Classified Particles

- GC-MS Analysis -



- PAH content decreases in the range of 10-56nm in diameter.